

## B. Ball Spline

[www.tbimotion.com.tw](http://www.tbimotion.com.tw)

# 1. About Ball Spline

## 1-1 Structure and Benefits of *TBI MOTION* Ball Spline

### 1-1-1 Basic Structure of *TBI MOTION* Ball Spline

The design of TBI Ball spline is to utilize the friction force through the contact of steel balls within in the Spline Nut and the grooves on the Spline Shaft. With TBI MOTION's unique 40° angular contact design which enables the Ball spline delivers high sensitivity and extreme high load carrying capacity. The concept is optimal for the application involve with high speed, vibrates, impacts of loading and precise positioning requirements. Also when the Ball spline is used to function as linear bushing, the Ball spline provides ten times loading capacity than the linear bushing in the like dimensioned but with a compact profile. Namely, Durability and reliability is the reason for choosing TBI Ball spline in your application.

### 1-1-2 *TBI MOTION* Nut Design and Shaft Specifications

*TBI MOTION* Spline Nut is available in two different designs: SLF (Flange design) and SLT (Non-flange design). Point of contacts on the Spline shaft is provided in two grooves (180°) (SLF/SLT6~20) and four grooves (70°) (SLF/SLT25~50) base on the diameter of the Spline shaft. Also TBI provides Hollow Spline shaft for alternative.

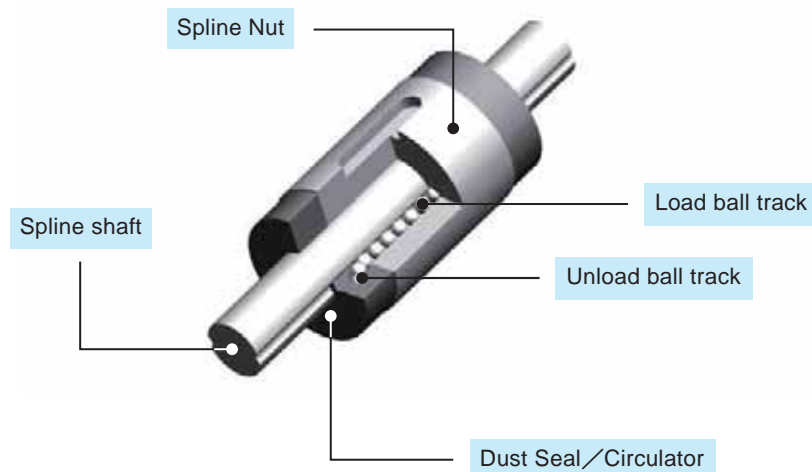


Fig 1.1.1

### 1-1-3 Features of *TBI MOTION* Ball Spline

#### High Load-Carrying Capacity

Every groove on the TBI Spline shaft is precision ground to form a perfect 40° angular contact point. The concept of 40° contact design is to increase the load carrying capacity and rigidity so that it is able to handle a greater moment load.

#### Zero Angular Clearance/Backlash

Every groove on the TBI Spline shaft is precision ground to form a perfect 40° angular contact point which is called the Gothic arch. The Gothic design eliminates clearance that could generate deflections and therefore best suited for the applications that require maximum precision.

#### High Sensitivity

The unique TBI 40° angular contact is design to drive with the minimum of friction force while the design performs not only the highest sensitivity but also the rigidity.

#### High Rigidity





A wide contact angle and an appropriate level of preload are combined to provide high torque and moment rigidity.

#### Mount-Simple on Design

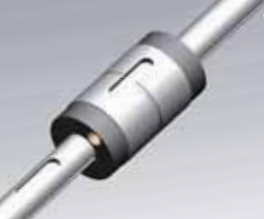


TBI Ball spline is low and simple maintenance designed, therefore even if disassembly is required. When the Spline Nut is necessary to remove for the spline shaft due to the ball retaining design the steel balls will not fall apart like the traditional Nut design.

1-1-4 TBI MOTION Ball Spline Type and Feature

Spline Nut

SLT, SOT Non-flanged Spline Nut	SLF, Flanged Spline Nut
	
<p>SLT, SOT Spline nut is with a straight cylindrical shape without flange. The standard mode of mounting a cylindrical nut is by using a key. The cylindrical nut will have a keyway and separate key. A matching keyway must be bored into the housing or block that will be mounted on the cylinder nut. The type SLT, SOT is the most compact profile Spline nut in TBI Ball Spline product line.</p>	<p>Flange nut is simpler to install, because it only requires a rough bore and mounting holes drilled and tapped to secure the flange to the housing.</p>
SZF, Flanged Spline Nut with Reinforced End Caps	SOF, Square Flanged Spline Nut
	
<p>The nut with reinforced end caps is suitable for the operation environment with high pollution. This is the design to avoid dirt going into the ball spline.</p>	<p>The nut with square flange is easy to be installed to the housing through mounting holes and will be applied to 3C industry and semiconductor industry.</p>

Spline Shaft

Standard Precision Spline Shaft	Hollow Spline Shaft (H-Type)	Custom Machining Spline Shaft
		
<p>The Standard precision Spline shaft is precisely ground to reach high accuracy and smoothness.</p>	<p>Hollow Spline shaft is optional for the customer to choose for its application. Hollow Spline shaft is design to reduce weight, accommodate pipes, ventilation.</p>	<p>Shaft shape. For example a shaft with a bigger diameter on both ends or on the center of Spline shaft can be manufactured upon request.</p>

1-2 The Procedure of Select Ball Spline

Table 1.2.1

Steps	Description
1. Set the Operational conditions	<ul style="list-style-type: none"> <li>Stroke Length : Ls</li> <li>Velocity : V</li> <li>The Applied Load : W</li> <li>Size</li> <li>Installation</li> <li>Use of the environment</li> <li>Service life expectancy</li> <li>Accuracy</li> <li>Frequency of use (load cycle)</li> <li>Rigidity</li> </ul>
2. Select a Type	<ul style="list-style-type: none"> <li>Refer to Type, Shaft Spec to determine the your Ball spline.</li> </ul>
3. Calculating the strength of Spline shaft	<ul style="list-style-type: none"> <li>Spline Shaft Diameter</li> <li>Spline-Shaft Length</li> <li>End Fixity</li> <li>The permissible load of Ball spline</li> <li>The displacement under torque and deflecting</li> </ul>
4. Service expectancy	<p>IF <span style="border: 1px solid black; padding: 2px;">Calculating TBI Ball spline service life expectancy by using expectancy formula.</span></p> <p>NO <span style="border: 1px solid black; padding: 2px;">NO Required service life.</span></p>
5. Determined the preload	<ul style="list-style-type: none"> <li>Determined the permissible axial clearance/backlash</li> </ul>
6. Determine the Accuracy Grade	<ul style="list-style-type: none"> <li>Accuracy Grades</li> </ul>
7. Operational condition	<ul style="list-style-type: none"> <li>Lubrication</li> <li>Lubrication methods</li> <li>Surface treatment</li> <li>Dust prevention methods</li> </ul>
Selected	

## 2. Technical Information

### 2-1 The Strength of Spline Shaft

The Spline shaft is designed to absorb radial load and torque during operation. Therefore, the strength of Spline shaft must be taken into consideration when the Ball spline operates under extreme loading or torque.

#### 2-1-1 The Bending Load Applied on the Operating Ball Spline

The maximum of bending moment (M) can be attributed to multi factors such as the end fixity methods, length of Spline shaft, load capacity, etc. Equation (1) is equipped to help the user to obtain the ideal length of the Spline shaft in order to be the reference of obtaining the ideal strength of Ball spline.

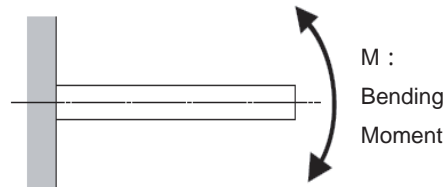


Fig 2.1.1

$$M = \sigma \cdot Z \text{ and } Z = \frac{M}{\sigma} \dots(1)$$

M : Bending moment (N-mm)

$\sigma$  : Shaft permissible bending stress (98 N/mm<sup>2</sup>)

Z : Shaft section modulus (mm<sup>3</sup>)

See Table 2.1.3, 2.1.4

#### 2-1-2 The Torque Applied on the Operating Ball Spline

The maximum torque applied on the Spline shaft can be calculated through maximum twisting moment (T). Equation (2) is equipped to help the user to obtain the ideal length of the Spline shaft in order to be the reference of obtaining the ideal strength of Ball spline.

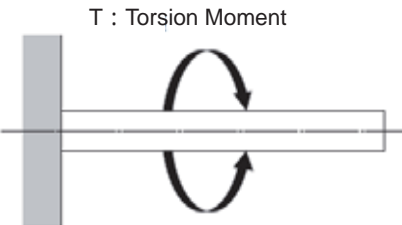


Fig 2.1.2

$$T = \tau_a \cdot Z_p \text{ and } Z_p = \frac{T}{\tau_a} \dots(2)$$

T : Maximum twisting moment (N · mm)

$\tau_a$  : Shaft permissible twisting Stress (49 N/mm<sup>2</sup>)

Z<sub>p</sub> : Shaft polar section modulus (mm<sup>3</sup>)

See Table 2.1.3, 2.1.4

#### 2-1-3 Both Bending Moment and Twisting Moment Applied Simultaneously on the Spline Shaft

To calculate the figure for both bending (M) and twisting moments (T) applied on the Spline shaft via equation (3) and (4) in order to get the equivalent bending moment (M<sub>e</sub>) and equivalent twisting moment (T<sub>e</sub>). Adopt the greater value from equation (3) and (4) to determine the ideal Spline-shaft length.

##### Equivalent Bending Moment

$$M_e = \frac{M + \sqrt{M^2 + T^2}}{2} = \frac{M}{2} \left\{ 1 + \sqrt{1 + \left(\frac{T}{M}\right)^2} \right\} \dots(3)$$

$$M_e = \sigma \cdot Z$$

##### Equivalent Twisting Moment

$$T_e = \sqrt{M^2 + T^2} = M \cdot \sqrt{1 + \left(\frac{T}{M}\right)^2} \dots(4)$$

$$T_e = \tau_a \cdot Z_p$$

#### 2-1-4 Rigidity of the Spline Shaft

The rigidity of the Spline Shaft is expressed in torsion angle caused by twisting moment. The twisting angle should be limited to no further than 0.25° per 1000 mm.

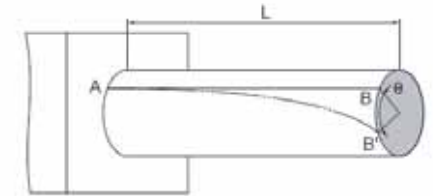


Fig 2.1.3

$$\theta = 57.3 \frac{T \cdot L}{G \cdot I_p} \dots(5)$$

$$\text{Shaft Rigidity} = \text{Torsion Angle} / \text{Unit Length} = \frac{\theta}{\ell} < \frac{1^\circ}{4}$$

$\theta$  : Torsion Angle (°)

L : Shaft Length (mm)

G : Transverse Elastic Modulus (7.9 · 10<sup>4</sup> N/mm<sup>2</sup>)

$\ell$  : Unit Length (1000mm)

I<sub>p</sub> : Polar Moment of Inertia I<sub>p</sub> (mm<sup>4</sup>)

See Table 2.1.3, 2.1.4

2-1-5 Deflection and Deflection Angle of the Spline Shaft

These should be calculated using equations satisfying the relevant operating conditions. Tables 2.1.1 & 2.1.2 present the operating conditions and the corresponding equations. Tables 2.1.3 & 2.1.4 presents the cross-section factors (Z) and cross-section secondary moments (I). Through the use of the Z, I values given in these tables, the strength and degree of displacement (deflection) of Ball spline model can be obtained.

Table 2.1.1 Deflection and Deflection-Angle Equation

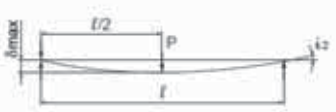
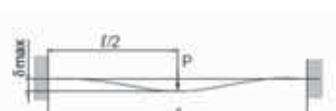
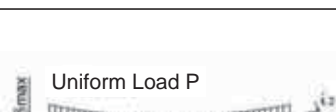


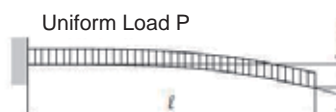
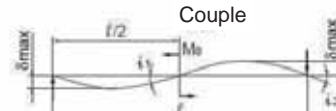
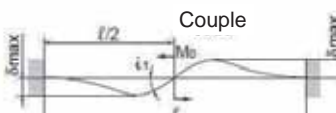
End Fixity	Specification Conditions	Deflection Equation	Deflection-Angle Equation
Both Ends Free		$\delta_{\max} = \frac{Pl^3}{48EI}$	$\begin{aligned} i_1 &= 0 \\ i_2 &= \frac{Pl^2}{16EI} \end{aligned}$
Both Ends Fixed		$\delta_{\max} = \frac{Pl^3}{192EI}$	$\begin{aligned} i_1 &= 0 \\ i_2 &= 0 \end{aligned}$
Both Ends Free		$\delta_{\max} = \frac{5Pl^4}{384EI}$	$\begin{aligned} i_1 &= 0 \\ i_2 &= \frac{Pl^3}{24EI} \end{aligned}$
Both Ends Fixed		$\delta_{\max} = \frac{Pl^4}{384EI}$	$i_2 = 0$

Table 2.1.2 Deflection and Deflection-Angle Equation

End Fixity	Specification Conditions	Deflection Equation	Deflection-Angle Equation
One Ends Free		$\delta_{\max} = \frac{Pl^3}{3EI}$	$\begin{aligned} i_1 &= \frac{Pl^2}{2EI} \\ i_2 &= 0 \end{aligned}$
One Ends Fixed		$\delta_{\max} = \frac{Pl^4}{8EI}$	$\begin{aligned} i_1 &= \frac{Pl^3}{6EI} \\ i_2 &= 0 \end{aligned}$
Both Ends Free		$\delta_{\max} = \frac{\sqrt{3}M_0l^2}{216EI}$	$\begin{aligned} i_1 &= \frac{M_0l}{12EI} \\ i_2 &= \frac{M_0l}{24EI} \end{aligned}$
Both Ends Fixed		$\delta_{\max} = \frac{M_0l^2}{216EI}$	$\begin{aligned} i_1 &= \frac{M_0l}{16EI} \\ i_2 &= 0 \end{aligned}$

$\delta_{\max}$  : Maximum Deflection (mm)

$i_1$  : Deflection Angle at a Loading Point (deg)

$i_2$  : Deflection Angle at a Supporting Point (deg)

$M_0$  : Moment (N-mm)

P : Concentrated Load (N)

p : Uniform Load (N/mm)

l : Span (mm)

I : Geometrical Moment of Inertia (mm<sup>4</sup>)

E : Longitudinal Elastic Modulus

(2.06 · 10<sup>5</sup> N/mm<sup>2</sup>)

2-1-6 Critical Speed of Spline Shaft

When an operating Ball spline reaches critical speed, the mechanical resonance occurs and no further operation can be performed under mechanical resonance. Namely, to keep Ball Spline under ideal operational, the speed limit must be kept under monitor. Therefore, to set an ideal operational speed for safety factor must be settled as 80% of critical speed as shown on equation (6)

Critical Speed

$$N_c = \frac{60 \lambda^2}{2 \pi \cdot \ell_b^2} \cdot \sqrt{\frac{E \cdot 10^3 \cdot I}{\gamma \cdot A}} \cdot 0.8 \dots (6)$$

$N_c$  : Critical Shaft Speed ( $\text{min}^{-1}$ )

$\ell_b$  : Center Distance (mm)

$E$  : Young's Modulus ( $2.06 \cdot 10^5 \text{ N/mm}^2$ )

$I$  : Moment of Inertia of the Shaft ( $\text{mm}^4$ )

$$I = \frac{\pi}{64} d_1^4 \quad d_1 : \text{Diameter (mm)}$$

$\gamma$  : Density(Specific Gravity)  
( $7.85 \cdot 10^{-6} \text{ kg/mm}^3$ )

$$A = \frac{\pi}{4} d_1^2 \quad d_1 : \text{Diameter (mm)}$$

$A$  : Spline-Shaft Cross-Sectional Area ( $\text{mm}^2$ )

$\lambda$  : Installation-Method-Dependent Factor

(Fig 2.1.4) Fixed-Free  $\lambda = 1.875$

(Fig 2.1.5) Supported-Supported  $\lambda = 3.142$

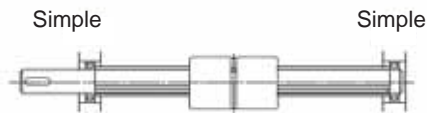
(Fig 2.1.6) Fixed-Supported  $\lambda = 3.927$

(Fig 2.1.7) Fixed-Fixed  $\lambda = 4.73$



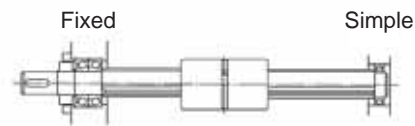
Fixed—Free

Fig 2.1.4



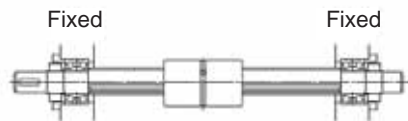
Simple — Simple

Fig 2.1.5



Fixed — Simple

Fig 2.1.6



Fixed — Fixed

Fig 2.1.7

2-1-7 Spline-Shaft Cross-Section

Table 2.1.3

Nominal Diameter		$I(\text{mm}^4)$	$I_p(\text{mm}^4)$	$Z(\text{mm}^3)$	$Z_p(\text{mm}^3)$
SL 006	Solid	63.49	119.23	18.58	39.74
	Hollow	62.70	117.33	18.32	39.22
SL 008	Solid	200.93	387.53	46.65	96.88
	Hollow	196.96	379.57	45.65	94.89
SL 010	Solid	490.25	933.29	86.61	186.66
	Hollow	477.68	908.16	86.10	181.63
SL 013	Solid	1400.81	2691.54	198.57	414.08
	Hollow	1282.96	2455.82	180.44	377.82
SL 016	Solid	3215.60	6242.70	378.39	780.34
	Hollow	3014.53	5840.57	353.25	730.07
SL 020	Solid	7851.80	15336.59	748.48	1533.66
	Hollow	7360.93	14354.84	699.39	1435.48
SL 025	Solid	18466.30	36932.60	1477.30	2954.61
	Hollow	15981.25	31962.50	1278.50	2557.00
SL 030	Solid	33122.31	77392.48	2579.75	4416.31
	Hollow	29905.32	70958.50	2365.28	3987.38
SL 032	Solid	50322.85	100645.70	3145.18	6290.36
	Hollow	36586.19	73172.38	2286.64	4573.27
SL 040	Solid	120667.43	241334.90	6033.37	12066.74
	Hollow	112813.45	225626.90	5640.67	11281.35
SL 050	Solid	297123.73	594247.50	11884.95	23769.90
	Hollow	274691.98	549384.00	10987.68	21975.36

$I$  : Geometrical moment of inertia ( $\text{mm}^4$ )       $I_p$  : Polar moment of inertia ( $\text{mm}^4$ )

$Z$  : Section modulus ( $\text{mm}^3$ )       $Z_p$  : Polar section modulus ( $\text{mm}^3$ )

Table 2.1.4

Nominal Diameter		I(mm <sup>4</sup> )	I <sub>p</sub> (mm <sup>4</sup> )	Z(mm <sup>3</sup> )	Z <sub>p</sub> (mm <sup>3</sup> )
SO 008	Solid	200.95	389.81	47.22	97.45
	Hollow	196.97	381.86	46.22	95.46
SO 010	Solid	490.68	956.77	93.22	191.35
	Hollow	478.11	931.64	90.71	186.33
SO 012	Solid	1017.67	1998.75	163.51	333.13
	Hollow	954.05	1871.52	152.91	311.92
SO 015	Solid	1678.22	3241.10	212.50	476.63
SO 020	Solid	5382.92	10422.07	553.75	1145.28
SO 025	Solid	12796.48	24659.94	1048.86	2182.30

I : Geometrical moment of inertia (mm<sup>4</sup>)    I<sub>p</sub> : Polar moment of inertia (mm<sup>4</sup>)  
 Z : Section modulus (mm<sup>3</sup>)                      Z<sub>p</sub> : Polar section modulus (mm<sup>3</sup>)

## 2-2 Service Life Expectancy

### 2-2-1 Nominal Life

TBI define the nominal life of Ball Spline as 90 % of the average running distance before flaking within in the Ball Spline on the same manufacture cycle. Please note that therefore the nominal life expectancy is only for reference use.

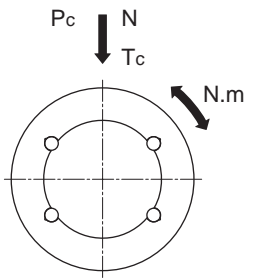


Fig 2.2.1

### 2-2-2 Calculating Nominal Life

The factors which influence the service life for Ball Splines can be attributed to three main aspects, the torque, radial load and moment. The influence of each aspect can be calculated through equations (7) to (10).

#### Under a Torque

$$L = \left( \frac{f_T \cdot f_C}{f_w} \cdot \frac{C_T}{T_C} \right)^3 \cdot 50 \dots(7)$$

#### Under a Radial Load

$$L = \left( \frac{f_T \cdot f_C}{f_w} \cdot \frac{C}{P_C} \right)^3 \cdot 50 \dots(8)$$

- L : Nominal Life (km)
- C<sub>T</sub> : Basic Dynamic-Torque (N-m)
- T<sub>C</sub> : Calculated Torque Applied (N-m)
- C : Basic Dynamic-Load Rating (N)
- P<sub>C</sub> : Radial Load (N)
- f<sub>T</sub> : Temperature (See Fig 2.2.2)
- f<sub>C</sub> : Contact (See Table 2.2.1)
- f<sub>w</sub> : Load Factor (See Table 2.2.2)

#### Under both a torque and radial load applied simultaneously

In this case, calculate the equivalent radial load to determine service life by equation. (9)

$$P_E = P_C + \frac{4 \cdot T_C \cdot 10^3}{BCD \cdot \cos \alpha} \dots(9)$$

- P<sub>E</sub> : Equivalent radial Load (N)
- α : Contact Angle
- i : Number of Loaded Rows of Balls
- BCD : Ball Center-to-Center Shaft Diameter (mm)
- (See Table 3.1.1)

#### Under a moment on one spline nut or two closely linked to one another

Obtain the equivalent radial load using the equation, and determine the service life by equation.(10)

- P<sub>u</sub> = K · M .....(10)
- P<sub>u</sub> : Equivalent Radial Load (N)(Moment Applied)
- K : Equivalent Factor (See Table 2.1.3)
- M : Applied Moment (N-mm)

Hower, M should be within the range of the stacic permissible moment.

#### Under both a moment and radial load applied simultaneously

Calculate the service life from the sum of the radial load and the equivalent radial load.



**Calculating Nominal Life**

Once the nominal life (L) is obtained, if the stroke length and the number of reciprocal operations are consistent, the service life in hours can be obtained by using the following equation.

$$L_h = \frac{L \cdot 10^3}{2 \cdot \ell_s \cdot n_1 \cdot 60} \dots\dots(11)$$

L<sub>h</sub> : Service Life in Hours (h)

ℓ<sub>s</sub> : Stroke Length (m)

n<sub>1</sub> : Number of Reciprocal Operations per Minute (min<sup>-1</sup>)

**Temperature Factor ( f<sub>T</sub> )**

When the Ball Spline operates in an environment which the temperature reaches 100°C or higher, considering that the heat may adversely affect the operation of the Ball Spline. To avoid malfunction under extreme temperature, Fig 2.2.2 should be taken into account. In addition that the material of Ball Spline should be heat resistant and custom made when use under extreme environment.

※Please inform TBI sales for upgrading the material for the operation environment exceeds 80°C for the reason that the materials of seal and retainers should be upgraded to sustain the high-temperature.※

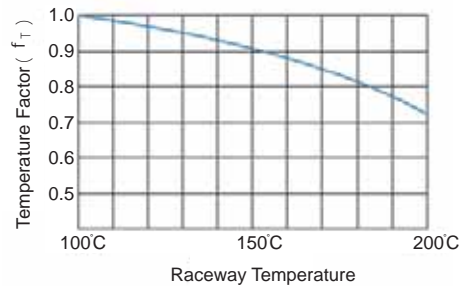


Fig 2.2.2 Temperature Factor ( f<sub>T</sub> )

**Contact Factor ( f<sub>C</sub> )**

When one or multiple Spline nuts mounts on the Spline shaft closely, their linear motion is affected by moments and mounting accuracy, resulting in nonuniform load distribution. When closely linked spline nuts are used, multiply the basic load rating ( C or Co ) by one of the contact factors specified below.

※If a non-uniform load distribution is expected, as in large equipment, take the contact factor explained in Table 4 into account.※

Table 2.2.1 Contact Factor ( f<sub>C</sub> )

No. of Spline nuts Linked	f <sub>C</sub>
2	0.81
3	0.72
4	0.66
5	0.61
In Normal Use	1.0

**Load Factor ( f<sub>w</sub> )**

The operation of reciprocal machines is likely to cause vibration and impact. It is difficult to determine the rating of vibration and impact in the event of vibration and repeated impact during high speed operation and triggering and ceasing of operation. Therefore, when loads exerted on a linear-motion or operation velocity and vibration is extreme. Take the basic load rating ( C or Co ) and multiply the figure shown in table 2.2.2

Table 2.2.2 Load Factor ( f<sub>w</sub> )

Vibration Impact	Velocity(V)	f <sub>w</sub>
Minor	Minor velocity V ≤ 0.25 m/s	1-1.2
Little	Low velocity 0.25 < V ≤ 1.0 m/s	1.2-1.5
Medium	Medium Velocity 1.0 < V ≤ 2.0 m/s	1.5-2.0
Heavy	High velocity V > 2.0 m/s	2.0-3.5

**2-2-3 Calculating the Average Applied Load**

The Applied load fluctuates during the operation of Ball Spline, For example, the applied load during the activities of an industrial robotic arm is different before holding a workpiece and return without it In a machine tool, the spline nut of the Ball Spline receives varying loads. Therefore, variables of the applied which influence the to calculate the service life of Ball Spline under on the hose-system operating conditions. The service life of the Ball Spline should therefore be calculated in consideration of such fluctuations in load. The mean load ( P<sub>m</sub> ) is the load under which the service life of the Ball Spline becomes equivalent to that under varying loads exerted on the spline nut while in operation.

The Equation is as below

$$P_m = \sqrt[3]{\frac{1}{L} \cdot \sum_{n=1}^n ( P_n^3 \cdot L_n )}$$

P<sub>m</sub> : Mean Load (N)

P<sub>n</sub> : Fluctuating Load (N)

L : Total Running Distance (mm)

L<sub>n</sub> : Running Distance Under Load P<sub>n</sub> (mm)

**For Loads That Change Stepwise**

$$P_m = \sqrt[3]{\frac{1}{L} ( P_1^3 \cdot L_1 + P_2^3 \cdot L_2 \dots P_n^3 \cdot L_n )}$$

P<sub>m</sub> : Mean Load (N)

P<sub>n</sub> : Fluctuating Load (N)

L : Total Running Distance (mm)

L<sub>n</sub> : Running Distance Under Load P<sub>n</sub> (mm)

**For Loads That Change Monotonically**

$$P_m = \frac{1}{3} ( P_{min} + 2 \cdot P_{max} )$$

P<sub>min</sub> : Minimum Load (N)

P<sub>max</sub> : Maximum Load (N)

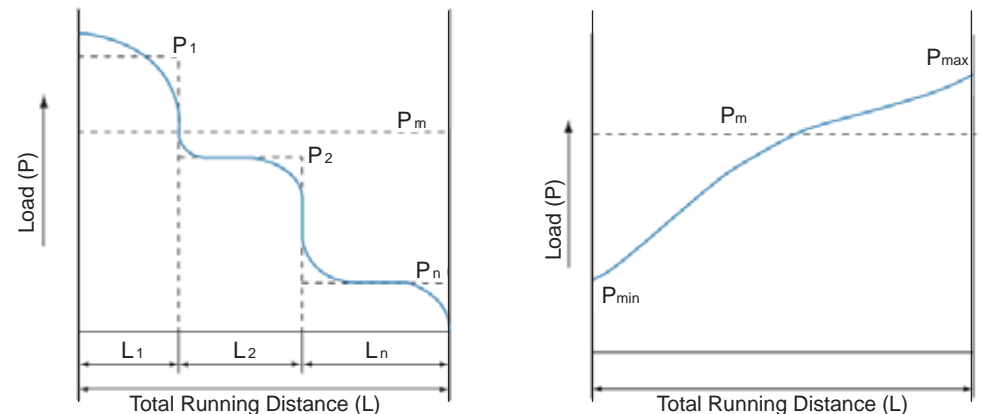


Fig 2.2.3

Fig 2.2.4



For Loads That Change Sinusoidal

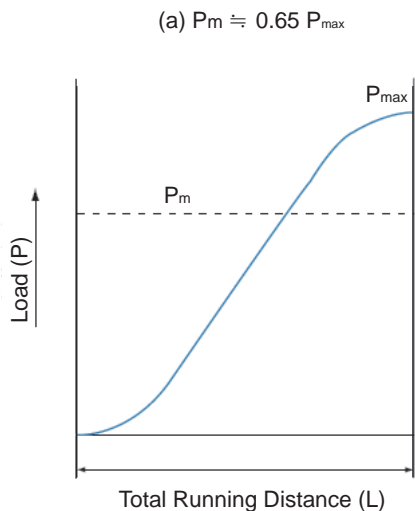


Fig 2.2.5

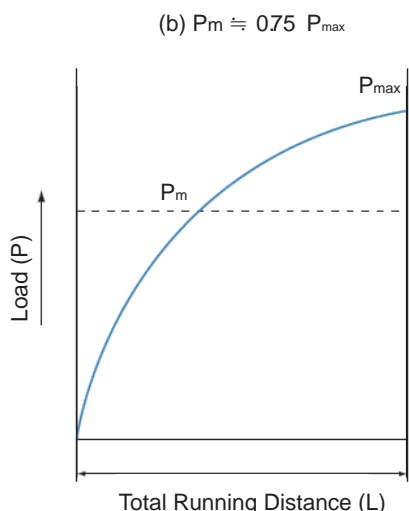


Fig 2.2.6

2-2-4 Equivalent Factor

Table 2.2.3 Equivalent Factor

Model No.	Equivalent Factor : K		Model No.	Equivalent Factor : K		Model No.	Equivalent Factor : K	
	One Spline Nut	Two Spline Nuts		One Spline Nut	Two Spline Nuts		One Spline Nut	Two Spline Nuts
SL 06	0.577	0.065	SZ 06	0.747	0.086	SO 08	0.400	0.061
SL 08	0.577	0.059	SZ 08	0.710	0.077	SO 10	0.308	0.052
SL 10	0.418	0.047	SZ 10	0.616	0.062	SO 12	0.253	0.046
SL 13	0.360	0.043	SZ 13	0.454	0.057	SO 15	0.219	0.040
SL 16	0.229	0.033	SZ 16	0.294	0.041	SO 20	0.186	0.031
SL 20	0.201	0.029	SZ 20	0.248	0.037	SO 25	0.154	0.026
SL 25	0.154	0.023	SZ 25	0.192	0.029			
SL 30	0.126	0.021	SZ 30	0.163	0.026			
SL 32	0.114	0.019	SZ 40	0.138	0.020			
SL 40	0.110	0.016	SZ 50	0.130	0.017			
SL 50	0.109	0.013						

2-3 Calculating the Service Life

Horizontal Application

A 300 mm long Ball Spline supported by two fixed nuts on each end setup for an horizontal application, the load of the Spline falls vertically downward on the fixed side with 30 mm away from the center of ball spline with the gravity force of  $W = 30$  kg. The figure is shown as Fig 2.3.1

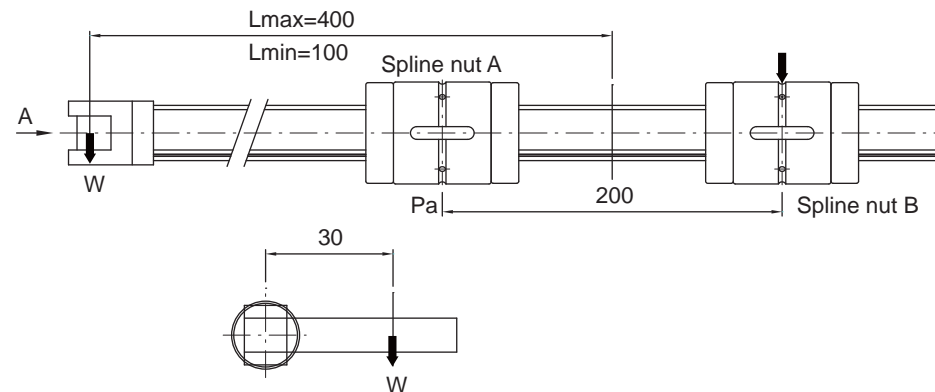


Fig 2.3.1

A. Calculates the Spline Shaft Strength

The present structure of ball spline is an extended bridge, it is designed to absorb torque, therefore the maxima bending load occurs on Spline nut A :

Maxima Bending Moment  $M = 30 \cdot 9.81 \cdot 400 = 117720$  N-mm

Maxima Torsion Moment  $T = 30 \cdot 9.81 \cdot 30 = 8829$  N-mm

For Ball Spline shafts subjected to the simultaneous application of torsion and bending loads, thus the calculation should include Equivalent Bending Moment,  $Me$  and Equivalent Torsion Moment  $Te$  :

$$Me = \frac{M + \sqrt{M^2 + T^2}}{2} = 117885 \text{ N-mm} \quad Te = \sqrt{M^2 + T^2} = 118051 \text{ N-mm}$$

$Te > Me$

$Te = Ta \cdot Zp$

$\therefore Zp = Te / Ta = 118051 / 49 = 2409.2 \text{ mm}^3$

According to figure of cross section showed on the spline ( Table2.1.3, 2.1.4 ), the minimum of 25 mm in diameter is required to in order to gain enough of strength for Ball Spline, therefore SLF25 matches the requirement above thus choose SLF25.

**B. Calculating the Mean Load**

When the bridge extension reached  $L_{max} = 400\text{mm}$ , it reaches its maxima load ( $P_{max}$ )

When it retrieved back to  $L_{min} = 100\text{mm}$ , it absorbed the minimum of load ( $P_{min}$ )

According to mechanics it allows us to find out the maxima and minimum Radial Load of Nut A and nut B :

$$P_{Amax} = 30 \cdot 9.81 \cdot (400+200)/200 = 882.9 \text{ N} \quad P_{Bmax} = 30 \cdot 9.81 \cdot 400/200 = 588.6 \text{ N}$$

$$P_{Amin} = 30 \cdot 9.81 \cdot (100+200)/200 = 441.5 \text{ N} \quad P_{Bmin} = 30 \cdot 9.81 \cdot 100/200 = 147.2 \text{ N}$$

When the movement of Ball Spline occurs, the load on the spline is gradual and repeated, according to Fig 2.2.4 the equation of the load on ball spline is shown as :

$$P_{Am} = 1/3 ( P_{Amin} + 2P_{Amax} ) = 735.8 \text{ N} \quad P_{Bm} = 1/3 ( P_{Bmin} + 2P_{Bmax} ) = 441.5 \text{ N}$$

The nuts receive both torsion and bending load simultaneously, therefore assuming that the torsion lies equally on the nuts. The equation for torsion is shown as T :

$$T' = T/2 = 30 \cdot 9.81 \cdot 30/2 = 4414.5 \text{ N-mm}$$

The equivalent factor  $P_e$  ( B12, equation (9) ) :

$$P_e = P_m + \frac{4 \cdot T'}{d_p \cdot \cos \alpha}$$

$$P_{AE} = 735.8 + \frac{4 \cdot 4414.5}{4 \cdot 27 \cdot \cos 50} = 990.2 \text{ N}$$

$$P_{BE} = 441.5 + \frac{4 \cdot 4414.5}{4 \cdot 27 \cdot \cos 50} = 695.9 \text{ N}$$

**C. Service Life Ball Spline**

$$\text{Nut A life } L_A = \left( \frac{f_T \cdot f_C}{f_w} \cdot \frac{C}{P_{AE}} \right)^3 \cdot 50 = 14518 \text{ km}$$

$$\text{Nut B life } L_B = \left( \frac{f_T \cdot f_C}{f_w} \cdot \frac{C}{P_{BE}} \right)^3 \cdot 50 = 41829 \text{ km}$$

Factors

$f_T$  : Temperature = 1

$f_C$  : Friction = 1

$f_w$  : Load = 1.5

C : Coa = 9835 N

The service life of Ball Spline is correlated with Nut A and the of service life is estimated as 14518 km.

**Vertical Application**

A 1200mm long ball spline with stroke of 1000 mm is mounted on a working platform supported by two fixed nuts on both end. The geometry is shown as Fig 2.3.2.

The point of drive force F is  $X_1 = 50 \text{ mm}$  from the center of Ball Spline, The weight platform  $W_1$  is 27 kg, The center of the weight is  $X_2 = 300 \text{ mm}$  away from the center of ball spline, The working cycle of platform is a carriage of  $W_2 = 5 \text{ kg}$  with a downward movement for 5 sec hold for 10 sec and elevation for 5 sec hold for 10 sec to unload the carriage repeatedly. The center of gravity of carriage is  $X_3 = 500 \text{ mm}$  from the center of ball spline, The travelling of velocity is shown as Fig 2.3.2.

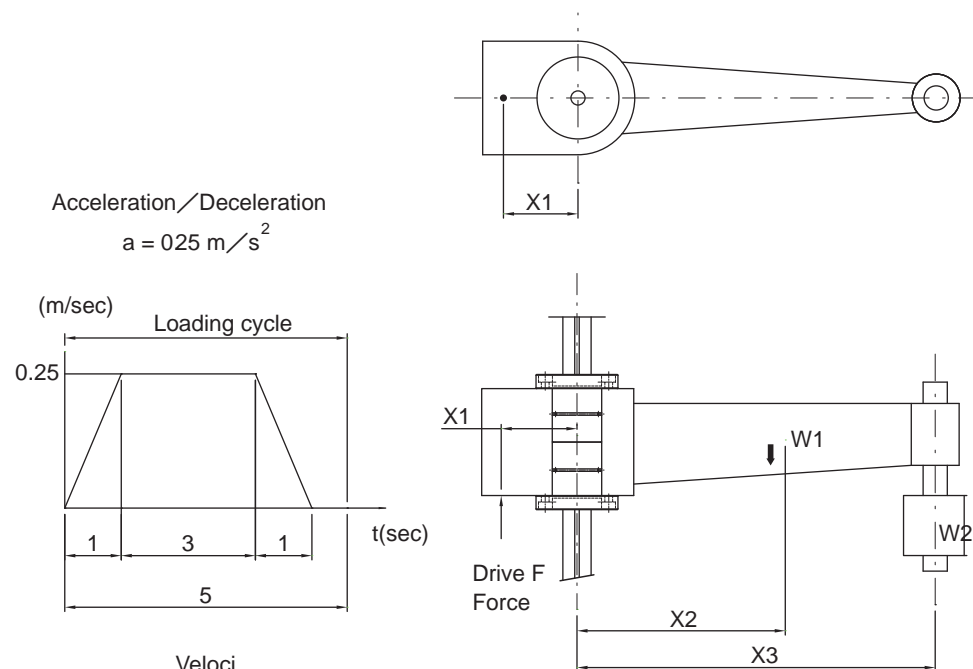


Fig 2.3.2

**A. Analysis on Different Stage of Exertion**

Inertial force occurs when a platform is in working modes, drive force is the source of the inertial force.

Inertial force of a  $m/s^2$  in acceleration ascent and deceleration decent :  $F = W \cdot (9.81+a)$

Inertial force of Constant velocity in acceleration and deceleration :  $F = W \cdot (9.81a)$

Inertial force of a  $m/s^2$  in acceleration decent and deceleration ascent :  $F = W \cdot (9.81-a)$

Below are the equations of the bending force absorb by the nuts during acceleration, constant velocity, deceleration while ball ascent and decent.

(1) (Without carriage)Acceleration while decent

$$Mda = W1 \cdot (9.81-a) \cdot 300 + W1 \cdot (9.81-a) \cdot 50 = 90342 \text{ N-mm}$$

(2) (Without carriage)constant velocity while decent

$$Mdc = W1 \cdot (9.81) \cdot 300 + W1 \cdot (9.81) \cdot 50 = 92704.5 \text{ N-mm}$$

(3) (Without carriage)deceleration while decent

$$Mdd = W1 \cdot (9.81+a) \cdot 300 + W1 \cdot (9.81+a) \cdot 50 = 95067 \text{ N-mm}$$

(4) (With carriage)acceleration while ascent

$$Maa = W1 \cdot (9.81+a) \cdot 300 + W1 \cdot (9.81+a) \cdot 50 + W2 \cdot (9.81+a) \cdot 500 + W2 \cdot (9.81+a) \cdot 50 = 122732 \text{ N-mm}$$

(5) (With carriage)constant velocity while ascent

$$Mac = W1 \cdot (9.81) \cdot 300 + W1 \cdot (9.81) \cdot 50 + W2 \cdot (9.81) \cdot 500 + W2 \cdot (9.81) \cdot 50 = 119682 \text{ N-mm}$$

(6) (With carriage)deceleration while ascent

$$Mad = W1 \cdot (9.81-a) \cdot 300 + W1 \cdot (9.81-a) \cdot 50 + W2 \cdot (9.81-a) \cdot 500 + W2 \cdot (9.81-a) \cdot 50 = 116632 \text{ N-mm}$$

**B. The Calculation of Spline Strength**

The present structure of ball spline is supported by two fixed nuts on both ends with an bridge of absorbing bending in the middle. it designed to absorb torque. According to mechanics the maxima bending load occurs on the supporting end. The Maxima Bending Moment should occur on at the end of acceleration.

$$\text{Maxima Bending Moment } M = 122732 \text{ N-mm}$$

$$\therefore Z = M/\sigma a = 122732/98 = 1252.4 \text{ mm}^3$$

According to figure of cross section showed on the spline, the minimum of 25 mm in diameter is required to in order to gain enough of strength for Ball Spline, therefore SLF25 matches the requirement above thus choose SLF25.

**C. Calculating the Mean Load**

The nuts and spline mainly affect by the force of bending, therefore represent ( B12, equation (10) ) by converting the force of bending into radial load.

$$Pn = K \cdot M$$

According to Table 2.1.6, when joint two SLF25 nuts, The equivalent factor  $K = 0.023$

$$Pda = 0.023 \cdot 90342 = 2078 \text{ N}$$

$$Paa = 0.023 \cdot 122732 = 2822.8 \text{ N}$$

$$Pdc = 0.023 \cdot 92704.5 = 2132.2 \text{ N}$$

$$Pac = 0.023 \cdot 119682 = 2752.7 \text{ N}$$

$$Pdd = 0.023 \cdot 95067 = 2186.5 \text{ N}$$

$$Pad = 0.023 \cdot 116632 = 2682.5 \text{ N}$$

The average load in every time period can be calculate as  $Pm$  :

$Pm = \sqrt[3]{\frac{1}{L} \cdot \sum_{n=1}^n (Pn^3 \cdot Ln)}$	$Pm$ : Average Load	(N)
	$Pn$ : Load in variable	(N)
	$L$ : Total service distances	(mm)
	$Ln$ : $Pn$ Service distances under loading	(mm)

$$Pm = \sqrt[3]{\frac{1}{1000} \{125 \cdot 2078^3 + 750 \cdot (2132.2)^3 + 125 \cdot (2822.8)^3 + 750 \cdot (2752.7)^3 + 125 \cdot (2682.5)^3\}}$$

$$= 2481.6 \text{ N}$$

### D. Analysis of Ball Spline Service Life

$$\text{Service Life } L = \left( \frac{f_T \cdot f_C}{f_W} \cdot \frac{C}{P_m} \right)^3$$

$$\cdot 50 = 922 \text{ km}$$

$f_T$  : Temperature = 1

$f_C$  : Friction = 1

$f_W$  : Load = 1.5

C : Coa = 9835 N

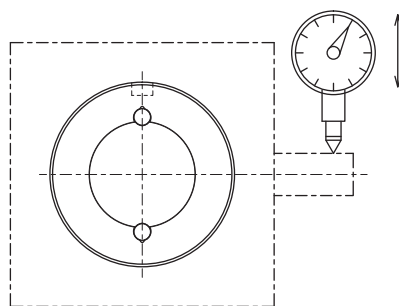


Fig 2.4.1

### 2-4 Determining the Preload

The preload a significant factor toward the accuracy, load resistance and rigidity of Ball Spline during operation. Therefore, it is very important to determine the most appropriate size of the clearance for your purpose of use. The size of the clearance is standardized for each type, enabling the one best-suited for operating conditions to be selected.

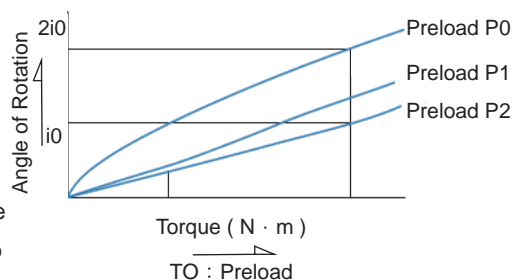


Fig 2.4.2

#### 2-4-1 Clearance in the Rotational Direction

With the Ball Spline, the sum of clearances in the circumferential direction is standardized as the clearance in the rotational direction. Clearance in the Rotational Direction (BCD)

#### 2-4-2 Preload and Rigidity

The preload is the load applied to balls prior to use for the purposes of eliminating angular backlash (clearance in the rotational direction) and improving rigidity. The application of a preload can eliminate angular backlash in the Ball Spline in accordance with the level of applied preload, and can improve rigidity. Fig 2.4.2 shows the amount of displacement in the rotational direction when a rotational torque is applied. As shown, the effect of preloading continues until the torque becomes Fig 2.4.2 times greater than the preload applied.

Compared with a setting without a preload, displacement at the same rotational torque is half that under a preload or less, and the rigidity is twice as great.

### 2-4-3 Operating Conditions and Determination of the Preload Level

Table 2.4.1 presents guidelines for determining the appropriate clearance in the rotational direction for the given operating conditions. The rotational clearance of the Ball Spline significantly affects the accuracy and rigidity of the Spline nut. Therefore, it is critical to select the clearance best suited for the intended uses of the Ball Spline. Normally, the Ball Spline in use is preloaded. When it is subjected to repeated swiveling and reciprocal linear motion, a system receives heavy vibration and impact. In such an environment, preloading prolongs the service life and improves accuracy.

Table 2.4.1 Guidelines for Determining an Appropriate Ball Spline Clearance according the Rotational Direction.

Clearance in the Rotational Direction	Preload	Operating conditions	Applications
	Medium Preload P2	<ul style="list-style-type: none"> <li>High rigidity is required. Vibration and impact are severe.</li> <li>The moment load must be borne by a single spline nut.</li> </ul>	<ul style="list-style-type: none"> <li>Construction-work-vehicle steering shaft.</li> <li>Spot-welding-machine shaft.</li> <li>Automatic-lathe-tool rest indexing shaft.</li> </ul>
Light preload P1	<ul style="list-style-type: none"> <li>Hanging loads and moments are applied.</li> <li>Highly reproducible accuracy is required.</li> <li>Alternate loads are applied.</li> </ul>	<ul style="list-style-type: none"> <li>Industrial robot arm Various automatic.</li> <li>loaders.</li> <li>Automatic-painting-machine guide shaft.</li> <li>Electric-discharge-machine spindle.</li> <li>Press die-set guide shaft.</li> <li>Drilling-machine spindle.</li> </ul>	
No preload P0	<ul style="list-style-type: none"> <li>Smooth movement should be achieved with only a low magnitude of force.</li> <li>Torque is continually applied in a given direction.</li> </ul>	<ul style="list-style-type: none"> <li>Various measuring instruments.</li> <li>Automatic drafting machine.</li> <li>Shape-measuring instrument.</li> <li>Dynamometer.</li> <li>Wire winder.</li> <li>Automatic arc cutter.</li> <li>Honing-machine spindle.</li> <li>Automatic packing machine.</li> </ul>	

Table 2.4.2 Ball spline Clearance in the Rotational Direction

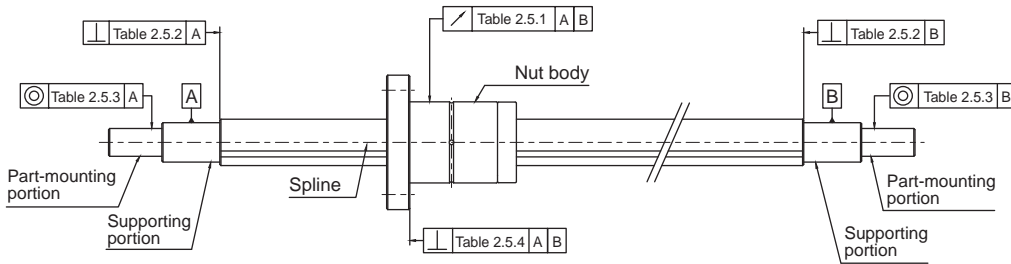
Unit :  $\mu\text{m}$

Nominal Diameter	Preload				No preload P0	Slight preload P1	Medium Preload P2	
	6	8	10	12	13			
15		16		20		-2 ~ +1	-6 ~ -2	-9 ~ -5
25			30			-3 ~ +2	-10 ~ -4	-14 ~ -8
40			50			-4 ~ +2	-16 ~ -8	-22 ~ -14

## 2-5 Accuracy

### 2-5-1 Accuracy Grade

The accuracy of the Ball Spline is determined by the callout of the spline-nut and thus divided into three accuracy grades of Normal(N), High(H), and Precision(P).



### 2-5-2 Accuracy Specifications

Tables 2.5.2~2.5.5 indicates the the measurement items of the Ball Spline.

Table 2.5.1 The Maximum Call Out of Spline Nut on the Support Unit Unit :  $\mu\text{m}$

Nominal Diameter		6, 8			10			13, 16, 20			25, 30			40, 50			
Length	Above	Below	Accuracy			Accuracy			Accuracy			Accuracy			Accuracy		
			N	H	P	N	H	P	N	H	P	N	H	P	N	H	P
-	-	200	72	46	26	59	36	20	56	34	18	53	32	18	53	32	16
200	200	315	133	89	57	83	54	32	71	45	25	58	39	21	58	36	19
315	315	400	185	126	82	103	68	41	83	53	31	70	44	25	63	39	21
400	400	500	236	163	108	123	82	51	95	62	38	78	50	29	68	43	24
500	500	630	-	-	-	151	102	65	112	-	-	88	57	34	74	47	27
630	630	800	-	-	-	190	130	85	-	-	-	103	68	42	84	54	32

Table 2.5.2 The Maximum Perpendicularity of Spline Shaft End on the Journal Ends Unit :  $\mu\text{m}$

Nominal Diameter		Accuracy		Normal (N)	High (H)	Precision (P)
6	8	10		22	9	6
12	13	15	16	20	11	8
25		30		33	13	9
40		50		39	16	11

Table 2.5.3 The Maximum Radial Call Out on the Attach Surface Unit :  $\mu\text{m}$

Nominal Diameter		Accuracy		Normal (N)	High (H)	Precision (P)
6	8			33	14	8
10				41	17	10
12	13	15	16	20	19	12
25		30		53	22	13
40		50		62	25	15

Table 2.5.4 The Perpendicularity of Flange on the Attach Surface Unit :  $\mu\text{m}$

Nominal Diameter		Accuracy		Normal (N)	High (H)	Precision (P)
6	8			17	11	8
10	12	13		33	13	9
15	16	20	25	30	16	11
40		50		46	19	13

Table 2.5.5 The Accuracy Level on the Effective Length Accuracy Unit :  $\mu\text{m}$

Accuracy	Normal (N)	High (H)	Precision (P)
Permissible	33	13	6

※Measurement according to any 100mm on the Spline shaft.※

BALL SPLINE

## 2-6 Lubrication

The spline nut is prelubricated prior to shipment for immediate use and the maintenance period is varied according to the operating conditions. TBI suggested that under normal operation condition re-lubricate your TBI Ball Spline after 100 kilometer or 6-12 months of operation. Apply lubricant within the nut body or on the groove of Spline shaft.

## 2-7 Material and Surface Treatment

*TBI MOTION* provides customize material and surface treatment in order to meet extreme operation condition. Please contact *TBI MOTION* service window for customized surface treatment and material.

## 2-8 Precautions of Ball Spline

### 2-8-1 General Maintenance

- (1) Disassemble ball spline without supervise of *TBI MOTION* certified engineer will casue malfunction on the ball spline.
- (2) Gravity causes the spline nut slides when lining the ball spline, handle with care.
- (3) DO NOT hammering, freefall the ball spline such action will damaging the ball spline and might hinder the performance of ball spline.
- (4) Prevent debris, scraps from intervene the ball spline cause it will decrease the performance to ball spline or lead to malfunction.
- (5) Prevent the ball spline operates under extreme condition. Contact *TBI MOTION* service window when the TBI ball spline is intend to use under extreme condition.
- (6) Coolant might casue malfunction on the ball spline, please contact *TBI MOTION* certified engineer for consulting the use of coolant.
- (7) Clean attached debris and scraps before relubrication.
- (8) Please contact *TBI MOTION* certified engineer for consulting when the ball spline is designed to operates under frequently vibrates, vacuum, extreme high and low temperature condition.
- (9) Please contact *TBI MOTION* certified engineer for consulting when mounting a through hole on the flanged ball spline.

### 2-8-2 Lubrication

- (1) Remove anti-dust oil before seal the ball spline with grease.
- (2) Prevent mix different kind of grease, it will cause unexpected chemical deform.
- (3) Please contact *TBI MOTION* certified engineer for consulting the use of grease when the ball spline is designed to operates under frequently vibrates, vacuum, extreme high and low temperature condition.
- (4) Please contact *TBI MOTION* certified engineer for consulting the use NON *TBI MOTION* certified grease.
- (5) When using of motor oil to serve the purpose of lubrication, it might cause performance declining due to the un-proper installation. Please contact *TBI MOTION* certified engineer for consulting.

### 2-8-3 Storage

Prevent extreme temperature and humidity when store ball spline, also use *TBI MOTION* certified seal and storage and it in a horizontal position.

## 2-9 Mounting

### 2-9-1 Tolerance on Support Unit

Ball spline nut and its support unit is bore to minimize the clearance. If high accuracy is not required, then a clearance fit can be used.

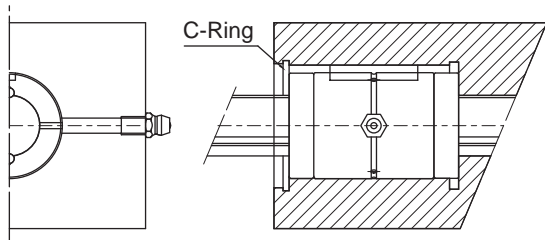
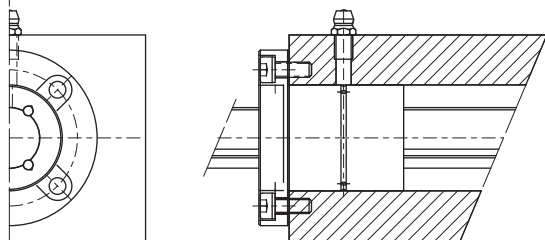
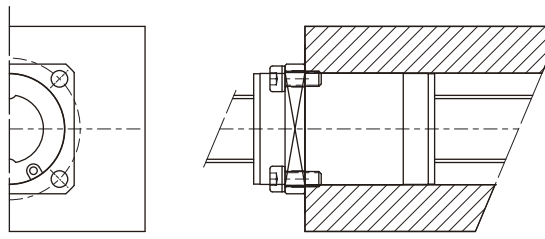
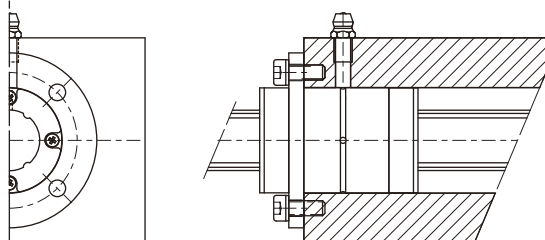
Table 2.9.1

Condition	Tolerance within Support Unit
General Operation Condition	H7
Operation Under Minimize of Axial Clearance	J6

2-9-2 Installation of Ball Spline

The installation of the ball spline is shown as Fig 2.9.2 Though the strength of mounting is not strictly standard, but it has to be certain that the the spline shaft has to be firmly fixed on the support unit.

Table 2.9.2 Sample of Spline-Nut Assembly

SLT, SOT (C-Ring Type)	
SLF (Flange One-Stage Type)	
SOF (Flange One-Stage Type)	
SZF (Flange One-Stage Type)	

2-9-3 Installation of Spline Nut

When intalling a spline nut into the spline shaft, use a jig like Fig 2.9.1 to insert the spline but with care.

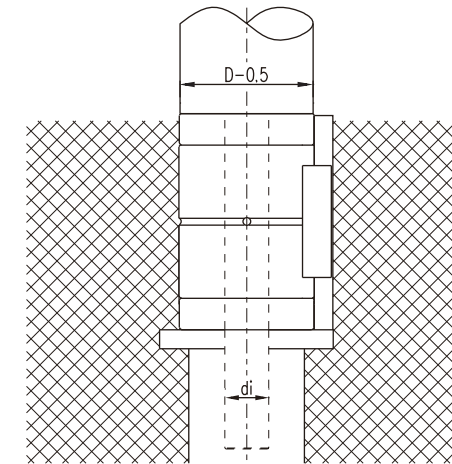


Fig 2.9.1

Table 2.9.3 Specifications of the jig

Unit : mm

Model	Nominal Diameter	6	8	10	13	16	20	25	30	40	50
SL, SZF	di	5.0	7.0	8.5	11.5	14.5	18.5	23	28	37.5	46.5
Model	Nominal Diameter	-	8	10	12	15	20	25	-	-	-
SO	di	-	7.0	8.5	10.5	11	16	20.5	-	-	-

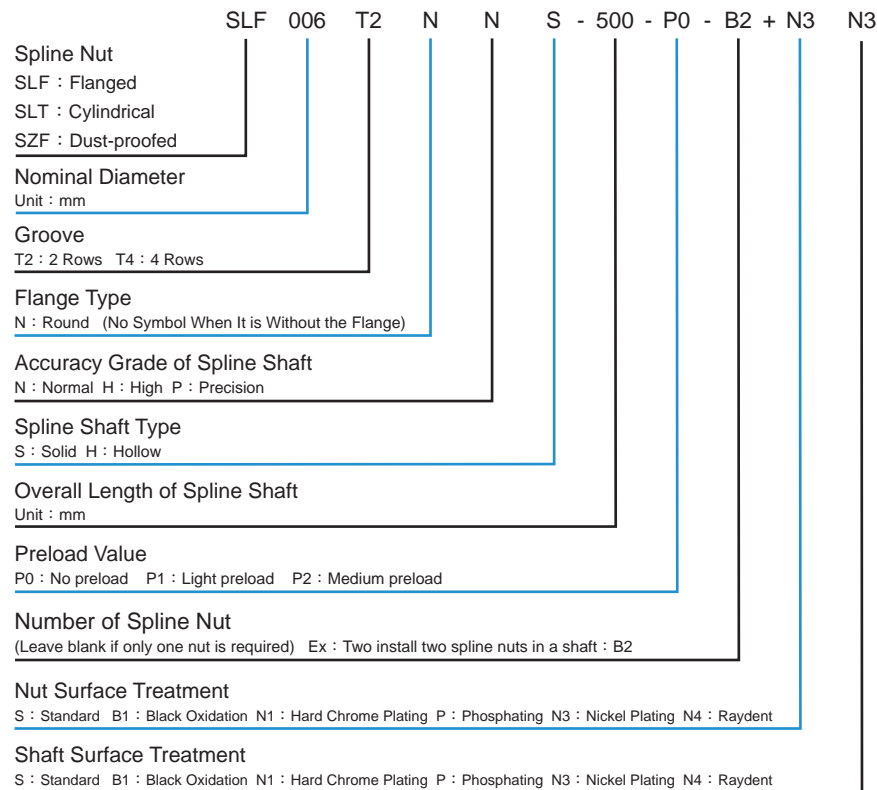


## 3-1 Nominal Model Code of Ball Spline SL, SZ Series

### 3-1-1 Nominal Model Code

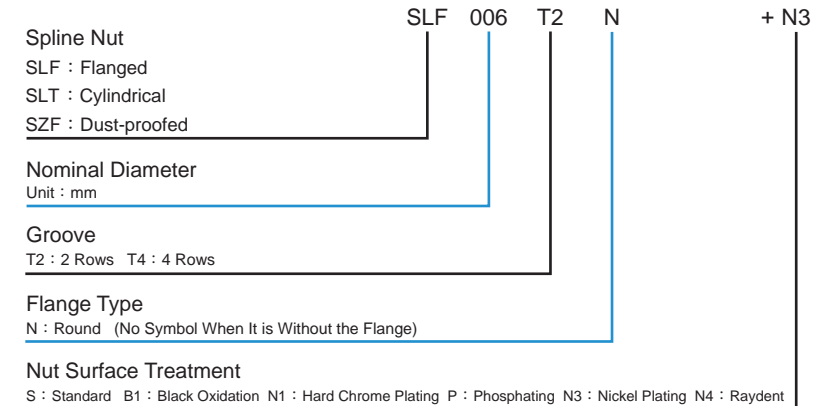
TBI MOTION ball Splines can be classified into interchangeable and non-interchangeable types. Their dimensions are the same; the only difference between the two types is that for non-interchangeable series, TBI MOTION will finish every process in the production line and hit customers' demands for preload and accuracy. Interchangeable nuts and shafts can be freely exchanged and the standard of the preload is P0. Customers could adjust the preload by changing the steel balls inside of the nut by themselves. It is very convenient for customers to have TBI MOTION ball splines in inventory and make the preload and end machining by themselves. TBI MOTION is proud of internal quality control process which is under strict international regulation.

#### Non-interchangeable Type Code :

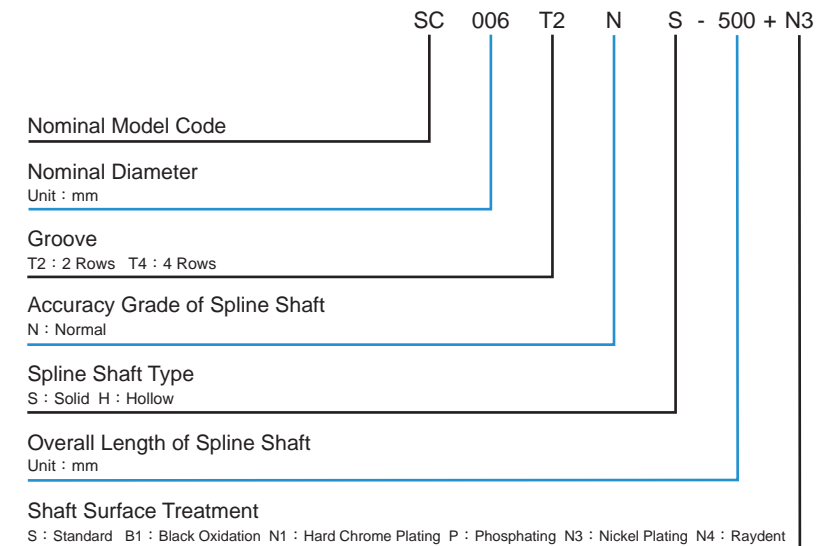


## Nominal Model Code for Interchangeable SL, SZ Type

### Interchangeable Type of Spline Nut :

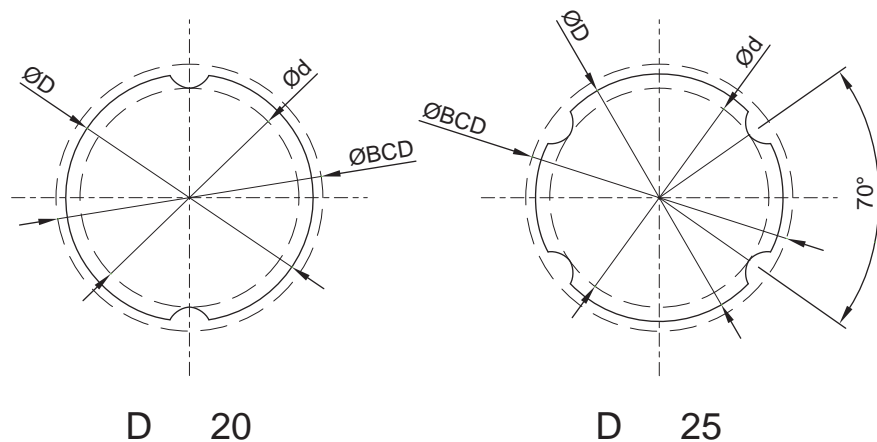


### Interchangeable Type of Spline Shaft :

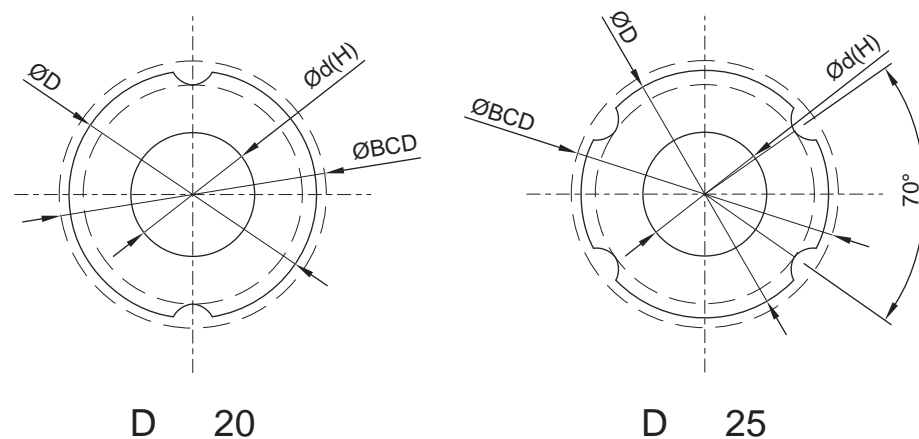


3-1-2 SLF, SLT, SZF Spline Shaft Cross-Sectional Shape

Table 3.1.1, 3.1.2 indicates the cross-section of spline shaft. When the shaft end is round pillar type the minor diameter must not be greater than the diameter of groove ridge.



Solid Spline Shaft



Hollow Spline Shaft

Table 3.1.1 Solid Spline Shaft Cross-Sectional Shape

Unit : mm

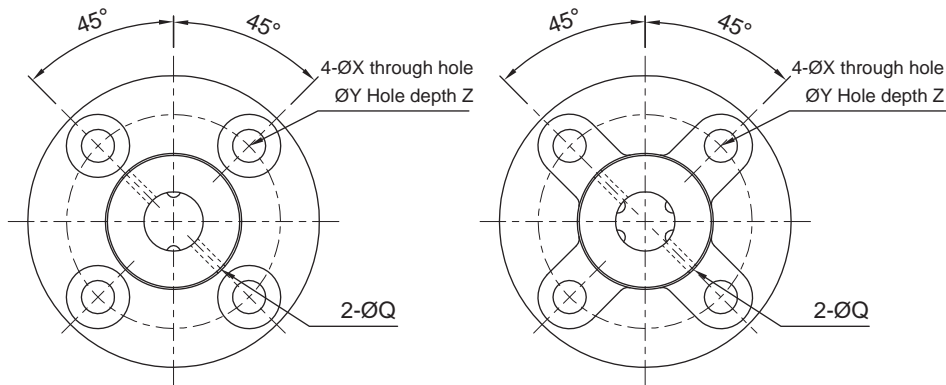
Nominal Diameter	6	8	10	13	16	20	25	30	40	50
Stats										
Inner Diameter Ød	5.25	7.27	8.97	11.82	14.72	18.63	23.43	28.53	37.3	47.05
Outer Diameter ØD h7	6	8	10	13	16	20	25	30	40	50
Mass(kg/m)	0.22	0.39	0.6	1.03	1.56	2.44	3.8	5.49	9.69	15.19
Ball Center ØBCD	6.75	8.77	11.35	14.6	17.5	21.8	27	32.1	43.65	54.2
Tolerance µm	0 -15	0 -15	0 -18	0 -18	0 -18	0 -21	0 -21	0 -25	0 -25	0 -30

Table 3.1.2 Hollow Spline Shaft Cross-Sectional Shape

Unit : mm

Nominal Diameter	6	8	10	13	16	20	25	30	40	50
Stats										
Inner Diameter Ød	2	3	4	7	8	10	15	16	20	26
Outer Diameter ØD h7	6	8	10	13	16	20	25	30	40	50
Mass(kg/m)	0.177	0.33	0.506	0.872	1.25	1.82	2.92	3.93	6.75	11.4
Ball Center ØBCD	6.75	8.77	11.35	14.6	17.5	21.8	27	32.1	43.65	54.2
Tolerance µm	0 -15	0 -15	0 -18	0 -18	0 -18	0 -21	0 -21	0 -25	0 -25	0 -30

SLF Series Specifications

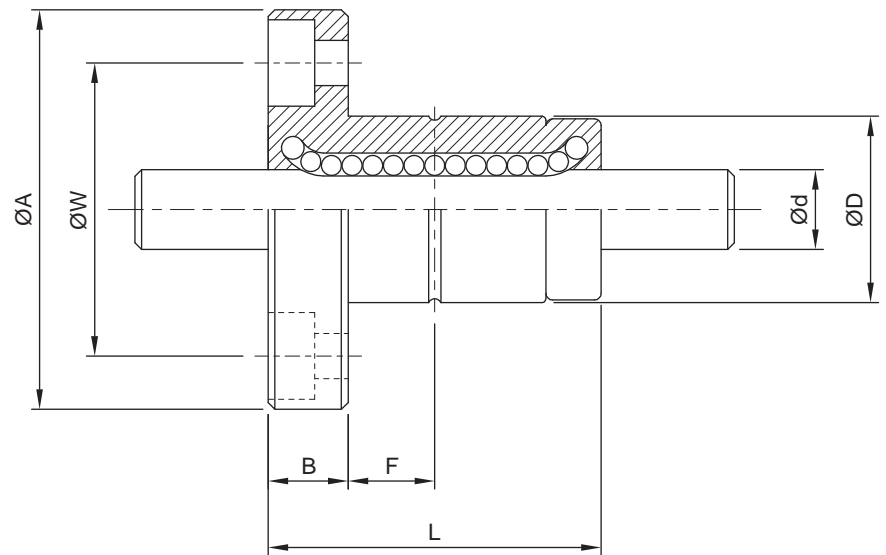


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Shaft diameter d 20

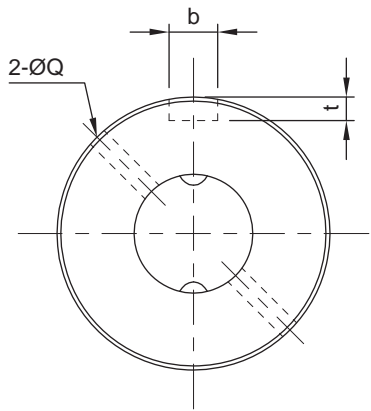
Shaft diameter d 25



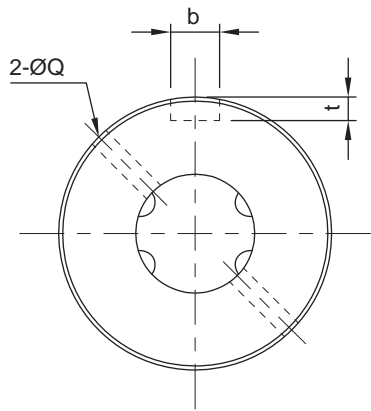
Model No.	Diameter		Row	Spline Nut Dimension							Mounting Hole X · Y · Z
	d	h7		D	L	A	B	F	Oil Q	W	
	SLF006	6			14	25	30	6	7.5	1	
SLF008	8		16	27	32	8	7.5	1.5	24	3.4 · 6.5 · 4.5	
SLF010	10		21	33	42	9	10.5	1.5	32	4.5 · 8 · 4	
SLF013	13		24	36	44	9	11	1.5	33	4.5 · 8 · 4.5	
SLF016	16		31	50	51	10	18	2	40	4.5 · 8 · 6	
SLF020	20		35	56	58	10	18	2	45	5.5 · 9.5 · 5.4	
SLF025	25		42	71	65	13	26.5	3	52	5.5 · 9.5 · 8	
SLF030	30		47	80	75	13	30	3	60	6.6 · 11 · 8	
SLF040	40		64	100	100	18	36	4	82	9 · 14 · 12	
SLF050	50		80	125	124	20	46.5	4	102	11 · 17.5 · 12	

Model No.	Basic Load Rating		Basic Torsion		Static Permissible Moment		Mass	
	C	C0	CT	C0T	MA1	MA2	Spline Nut	Spline Shaft
	kgf	kgf	kgf · m	kgf · m	kgf · m	kgf · m	g	kg/m
SLF006	137	225	0.46	0.76	0.39	3.48	36.7	0.22
SLF008	137	225	0.60	0.99	0.39	3.82	47	0.39
SLF010	285	397	1.62	2.25	0.95	8.53	100	0.60
SLF013	396	540	2.89	3.94	1.50	12.46	117	1.03
SLF016	545	849	4.77	7.43	3.71	26.09	226	1.56
SLF020	724	1109	7.90	12.09	5.53	38.00	303	2.44
SLF025	1003	1593	21.99	43.01	10.35	68.59	458	3.80
SLF030	1160	1980	30.26	62.93	15.68	93.27	633	5.49
SLF040	2972	4033	105.37	176.05	36.59	246.34	1430	9.69
SLF050	4086	5615	179.89	304.35	51.58	428.72	2756	15.19

SLT Series Specifications



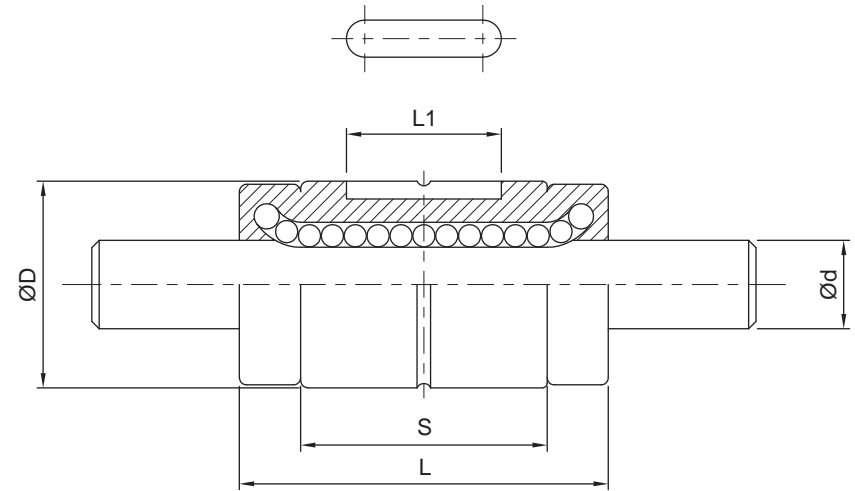
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Shaft diameter d 20

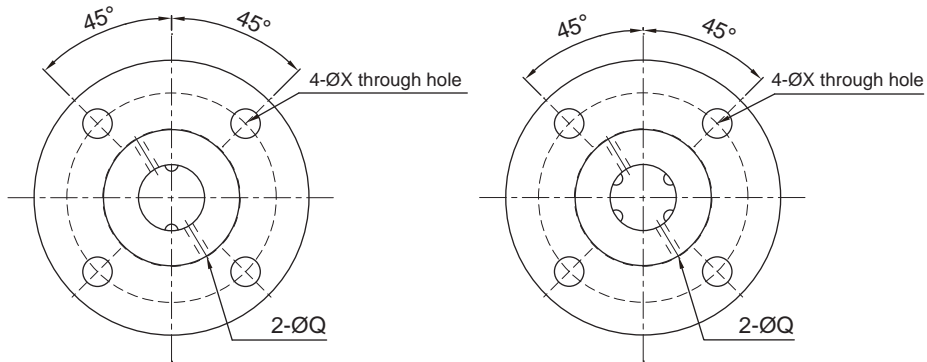
Shaft diameter d 25



Model No.	Diameter		Spline Nut Dimension				Keyway Dimensions		
	d	h7	D	L	S	L1	Oil	b	t
							Q	H8	$+0.05$ $-0$
SLT006	6	2	14	25	16.7	10.5	1	2.5	1.2
SLT008	8	2	16	27	15.7	10.5	1.5	2.5	1.2
SLT010	10	2	21	33	20	13	1.5	3	1.5
SLT013	13	2	24	36	23	15	1.5	3	1.5
SLT016	16	2	31	50	34	17.5	2	3.5	2
SLT020	20	2	35	56	39.7	29	2	4	2.5
SLT025	25	4	42	71	50.3	36	3	4	2.5
SLT030	30	4	47	80	60	42	3	4	2.5
SLT040	40	4	64	100	70	52	4	6	3.5
SLT050	50	4	80	125	91	58	4	8	4

Model No.	Basic Load Rating		Basic Torsion		Static Permissible Moment		Mass	
	C	C <sub>0</sub>	C <sub>T</sub>	C <sub>0T</sub>	MA1	MA2	Spline Nut	Spline Shaft
	kgf	kgf	kgf · m	kgf · m	kgf · m	kgf · m	g	kg/m
SLT006	137	225	0.46	0.76	0.39	3.48	14	0.22
SLT008	137	225	0.60	0.99	0.39	3.82	16	0.39
SLT010	285	397	1.62	2.25	0.95	8.53	37	0.60
SLT013	396	540	2.89	3.94	1.50	12.46	52	1.03
SLT016	545	849	4.77	7.43	3.71	26.09	130	1.56
SLT020	724	1109	7.90	12.09	5.53	38.00	188	2.44
SLT025	1003	1593	21.99	43.01	10.35	68.59	285	3.80
SLT030	1160	1960	30.26	62.93	15.68	93.27	395	5.49
SLT040	2972	4033	105.37	176.05	36.59	264.34	843	9.69
SLT050	4086	5615	179.89	304.35	51.58	428.72	1758	15.19

SZF Series Specifications

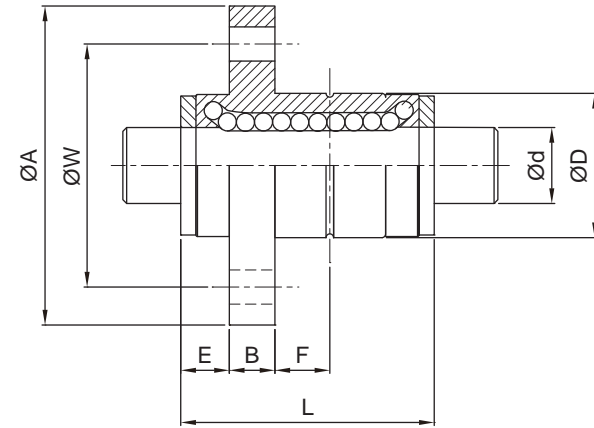


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Shaft diameter d 20

Shaft diameter d 25



Model No.	Diameter		Spline Nut Dimension								
	d	h7	D	L	A	B	E	F	Oil	W	Mounting Hole
									Q		X
SZF006	6		14	25	30	3	5.7	4	1	22	3.4
SZF008	8		16	27	32	3	7.2	4	1.5	24	3.4
SZF010	10		21	33	42	4	8	5	1.5	32	4.5
SZF013	13		24	36	44	5	8	6	1.5	33	4.5
SZF016	16		31	50	51	5	9.5	12	2	40	4.5
SZF020	20		35	56	58	5	9.7	15	2	45	5.5
SZF025	25		42	71	65	6	11.9	20	3	52	5.5
SZF030	30		47	80	75	6	12	24	3	60	6.6
SZF040	40		64	100	100	8	17	27	4	82	9
SZF050	50		80	125	124	10	19.5	40	4	102	11

Model No.	Basic Load Rating		Basic Torsion		Static Permissible Moment		Mass	
	C	C0	CT	C0T	MA1	MA2	Spline Nut	Spline Shaft
	kgf	kgf	kgf · m	kgf · m	kgf · m	kgf · m	g	kg/m
SZF006	100	142	0.34	0.49	0.19	1.65	25	0.22
SZF008	100	142	0.44	0.62	0.20	1.86	28	0.39
SZF010	233	314	1.32	1.78	0.51	5.04	64	0.60
SZF013	342	463	2.50	3.38	1.02	8.08	87	1.03
SZF016	469	728	4.10	6.37	2.48	17.79	179	1.56
SZF020	653	951	7.12	10.37	3.84	26.00	240	2.44
SZF025	943	1517	20.68	40.97	7.89	53.18	385	3.80
SZF030	1089	1868	28.39	59.95	11.49	72.54	529	5.49
SZF040	2854	3842	101.19	167.72	27.87	190.46	1151	9.69
SZF050	4086	5615	179.89	304.35	43.03	323.43	2348	15.19

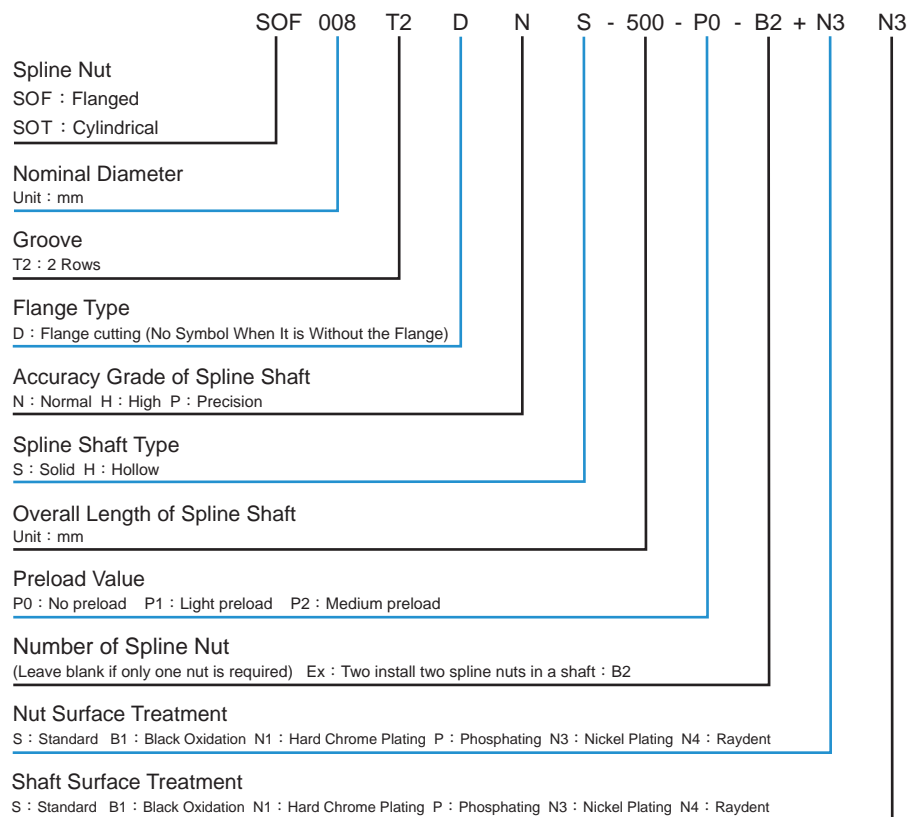
BALL SPLINE

### 3-2 Nominal Model Code of Ball Spline SO Series

#### 3-2-1 Nominal Model Code

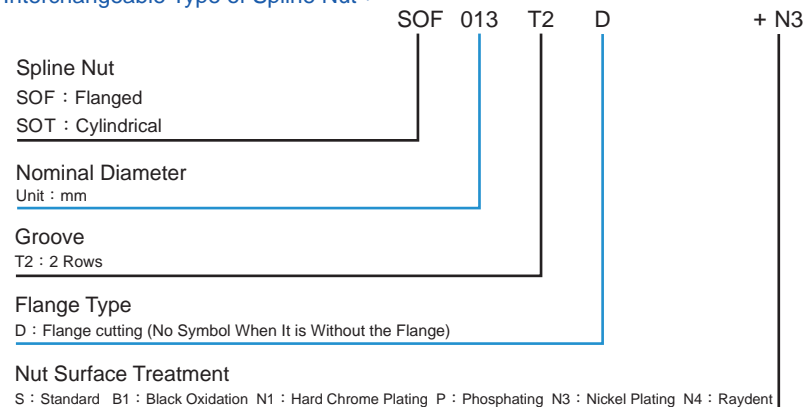
**TBI MOTION** ball Splines can be classified into interchangeable and non-interchangeable types. Their dimensions are the same; the only difference between the two types is that for non-interchangeable series, **TBI MOTION** will finish every process in the production line and hit customers' demands for preload and accuracy. Interchangeable nuts and shafts can be freely exchanged and the standard of the preload is P0. Customers could adjust the preload by changing the steel balls inside of the nut by themselves. It is very convenient for customers to have **TBI MOTION** ball splines in inventory and make the preload and end machining by themselves. **TBI MOTION** is proud of internal quality control process which is under strict international regulation.

#### Non-interchangeable Type Code :

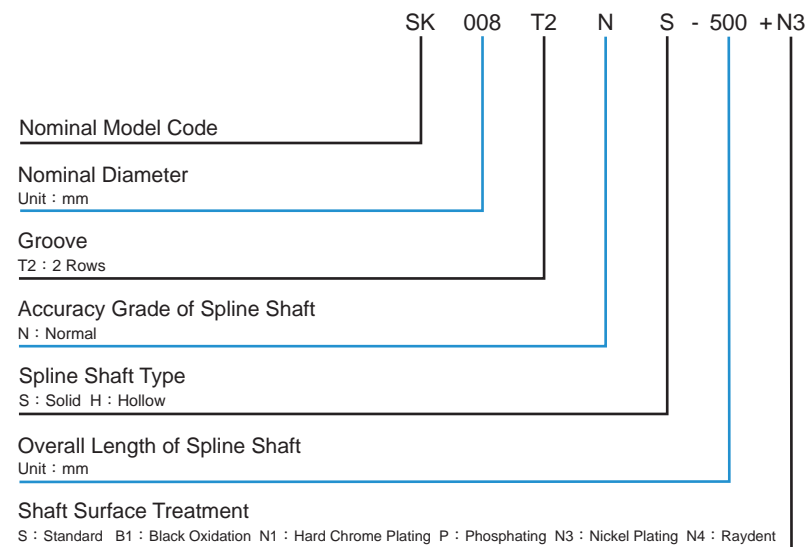


### Nominal Model Code for Interchangeable SO Type

#### Interchangeable Type of Spline Nut :

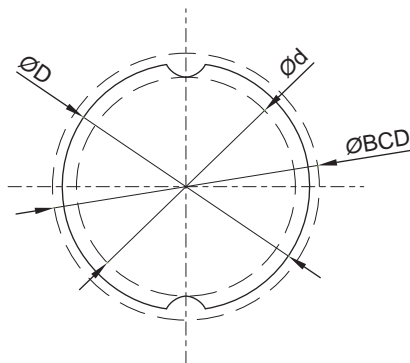


#### Interchangeable Type of Spline Shaft :

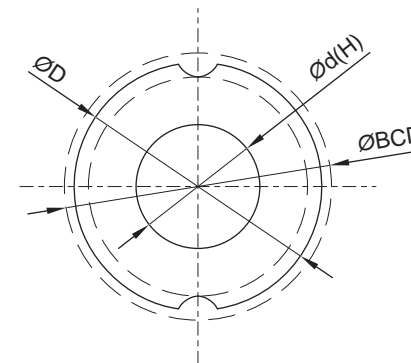


BALL SPLINE

3-2-2 SOF, SOT Spline Shaft Cross-Sectional Shape



Solid Spline Shaft



Hollow Spline Shaft

Table 3.2.1 Solid Spline Shaft Cross-Sectional Shape Unit : mm

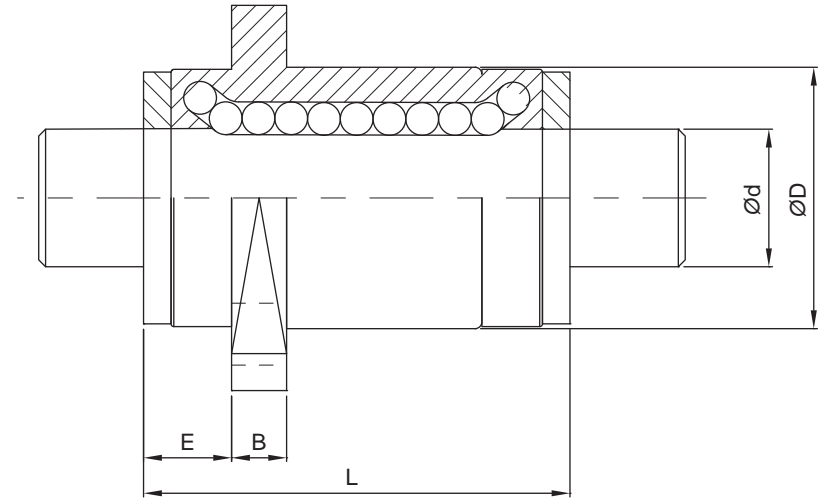
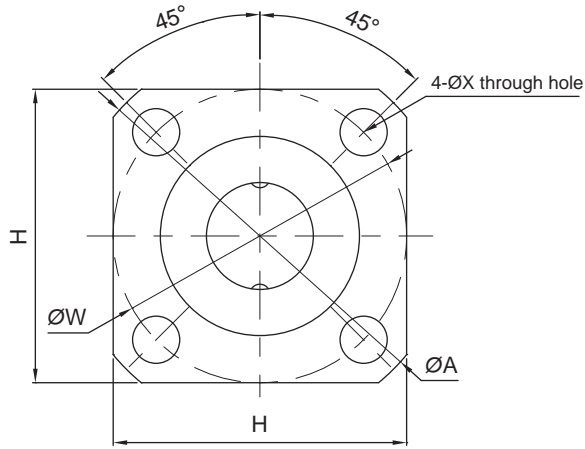
Nominal Diameter	8	10	12	15	20	25
Inner Diameter Ød	7	8.9	10.9	11.6	15.7	19.4
Outer Diameter ØD h7	8	10	12	13.6	18.2	22.6
Mass(kg/m)	0.39	0.605	0.875	1.11	2.02	3.1
Ball Center ØBCD	9.3	11.6	13.6	15	20	25
Tolerance µm	0 -15	0 -18	0 -18	0 -18	0 -21	0 -21

Table 3.2.2 Hollow Spline Shaft Cross-Sectional Shape Unit : mm

Nominal Diameter	8	10	12
Inner Diameter Ød	3	4	6
Outer Diameter ØD h7	8	10	12
Mass(kg/m)	0.33	0.51	0.66
Ball Center ØBCD	9.3	11.6	13.6
Tolerance µm	0 -15	0 -18	0 -18



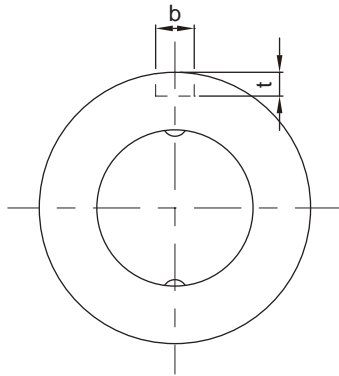
SOF Series Specifications



Model No.	Diameter		Row	Spline Nut Dimension							Mounting Hole X
	d	h7		D	L	A	B	E	F	W	
	SOF008	8		2	15	25	28	3.8	5.2	22	
SOF010	10	2	19	30	36	4.1	5.9	28	28	4.5	
SOF012	12	2	21	35	38	4	6	30	30	4.5	
SOF015	13.6	2	23	40	40	4.5	6.5	31	32	4.5	
SOF020	18.2	2	30	50	46	5.5	8.5	35	38	4.5	
SOF025	22.6	2	37	60	57	6.6	10.4	43	47	5.5	

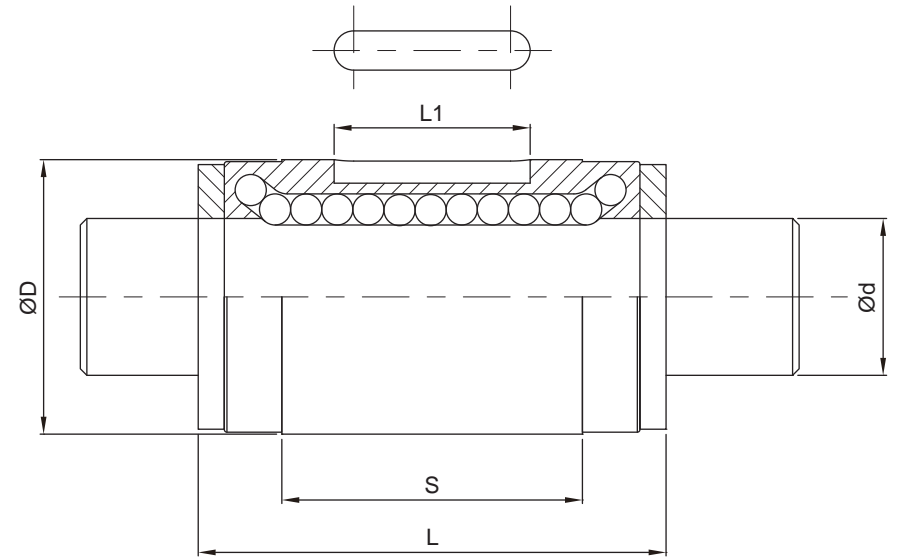
Model No.	Basic Load Rating		Basic Torsion		Static Permissible Moment		Mass	
	C	C0	CT	C0T	MA1	MA2	Spline Nut	Spline Shaft
	kgf	kgf	kgf · m	kgf · m	kgf · m	kgf · m	g	kg/m
SOF008	121	136	0.56	0.63	0.34	2.24	23.5	0.39
SOF010	192	219	1.11	1.27	0.71	4.23	45	0.61
SOF013	222	274	1.51	1.87	1.08	6.02	59	0.88
SOF016	426	619	3.19	4.65	2.83	15.49	77	1.11
SOF020	673	922	6.73	9.22	4.95	29.36	150	2.02
SOF025	1142	1458	14.17	18.14	9.46	56.17	255	3.10

SOT Series Specifications



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Shaft diameter



BALL SPLINE

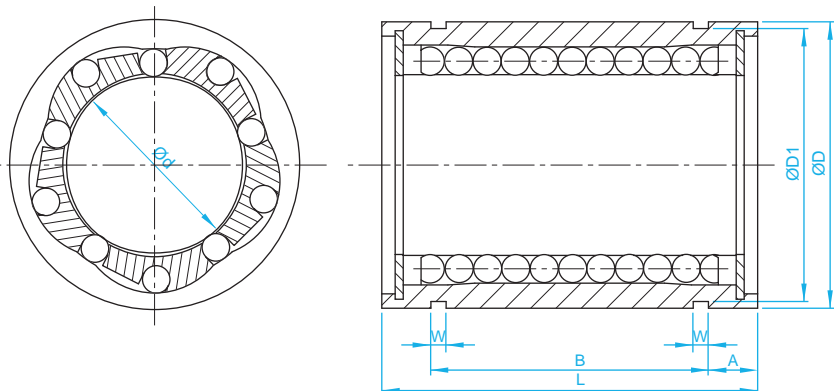
Model No.	Diameter		Row	Spline Nut Dimension				Keyway Dimensions	
	d	h7		D	L	S	L1	b	t
	H8							$+0.05$ $-0$	
SOT008	8	2	15	25	14.6	8.5	2.5	1.5	
SOT010	10	2	19	30	18.2	11	3	1.8	
SOT012	12	2	21	35	23	15	3	1.8	
SOT015	13.6	2	23	40	27	20	3.5	2	
SOT020	18.2	2	30	50	33	26	4	2.5	
SOT025	22.6	2	37	60	39.2	29	5	3	

Model No.	Basic Load Rating		Basic Torsion		Static Permissible Moment		Mass	
	C	C0	CT	C0T	MA1	MA2	Spline Nut	Spline Shaft
	kgf	kgf	kgf · m	kgf · m	kgf · m	kgf · m	g	kg/m
SOT008	121	136	0.56	0.63	0.34	2.24	15.9	0.39
SOT010	192	219	1.11	1.27	0.71	4.23	31.5	0.61
SOT012	222	274	1.51	1.87	1.08	6.02	44	0.88
SOT015	426	619	3.19	4.65	2.83	15.49	59.5	1.11
SOT020	673	922	6.73	9.22	4.95	29.36	130	2.02
SOT025	1142	1458	14.17	18.14	9.46	56.17	220	3.10

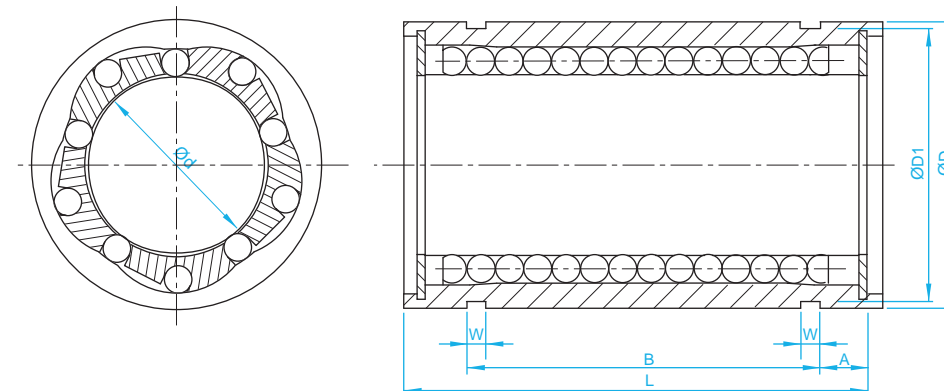
## E. Linear Ball Bearing

# 1. About Linear Ball Bearing

## LM Series Specifications (Standard)



## LM-L Series Specifications (Lengthen)



Unit : mm

Model No.	Dimension									Ca (kgf)	Coa (kgf)	Weight(g)
	d	D	D Tolerance (μm)	L	L Tolerance (μm)	W	D1	B	A			
LM-04UU	4	8	0	12	0	-	-	-	-	9	13	2
LM-06UU	6	12		19		1.1	11.5	13.5	2.75	21	27	8
LM-08UU	8	15	-11	24	0	1.1	14.3	17.5	3.25	27	41	16
LM-10UU	10	19		29		1.3	18	22	3.5	38	56	30
LM-12UU	12	21	-13	30	-20	1.3	20	23	3.5	42	61	31.5
LM-16UU	16	28		37		1.6	27	26.5	5.25	79	120	69
LM-20UU	20	32	0	42	0	1.6	30.5	30.5	5.75	88	140	87
LM-25UU	25	40		59		1.85	38	41	9	100	159	220
LM-30UU	30	45	-16	64	0	1.85	43	44.5	9.75	159	279	250
LM-40UU	40	60		80		2.1	57	60.5	9.75	219	409	585
LM-50UU	50	80	-19	100	-30	2.6	76.5	74	13	389	808	1580

※UU with oil seals in ends ※

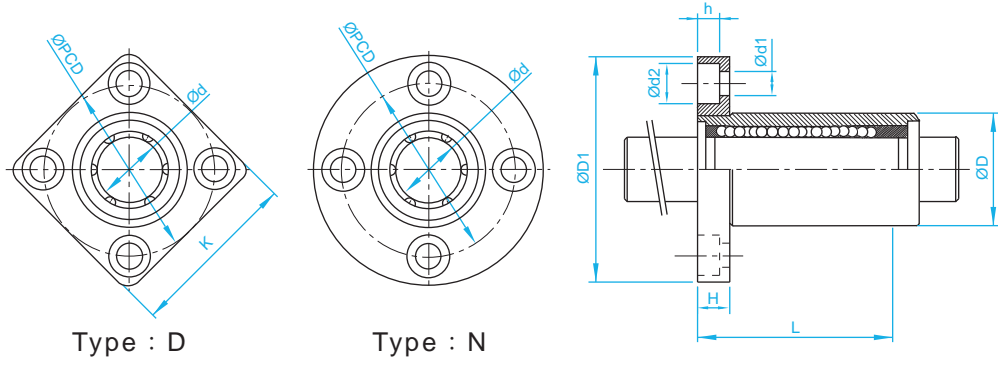
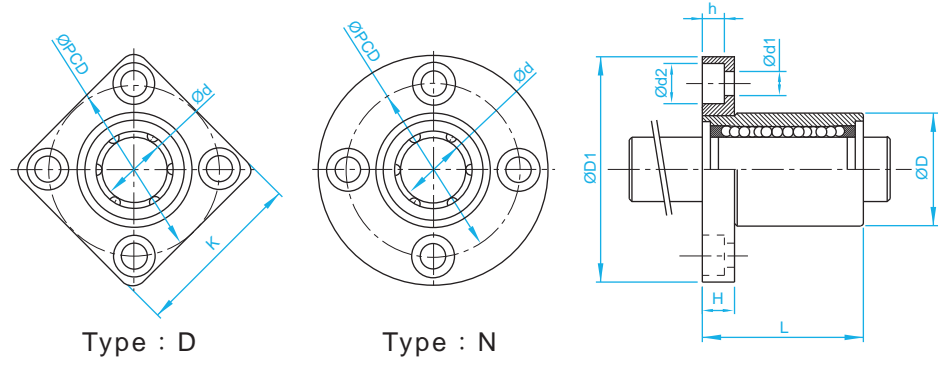
Unit : mm

Model No.	Dimension									Ca (kgf)	Coa (kgf)	Weight(g)
	d	D	D Tolerance (μm)	L	L Tolerance (μm)	W	D1	B	A			
LM-06LUU	6	12	0	35	0	1.1	11.5	27	4	33	54	16
LM-08LUU	8	15		-13		45	1.1	14.3	35	5	44	80
LM-10LUU	10	19	0	55	-30	1.3	18	44	5.5	60	112	62
LM-12LUU	12	21		57		1.3	20	46	5.5	83	160	80
LM-16LUU	16	28	-16	70	0	1.6	27	53	8.5	126	240	145
LM-20LUU	20	32		80		1.6	30.5	61	9.5	143	280	180
LM-25LUU	25	40	0	112	0	1.85	38	82	15	159	320	440
LM-30LUU	30	45		123		1.85	43	89	17	254	560	580
LM-40LUU	40	60	0	151	-40	2.1	57	121	15	350	820	1170
LM-50LUU	50	80		192		2.6	76.5	148	22	620	1622	3100

※UU with oil seals in ends ※

LF Series Specifications (Flange Type)

LF-L Series Specifications (Flange Type with Lengthen Nut)



Unit : mm

Unit : mm

Model No.	Dimension											Ca (kgf)	Coa (kgf)	Weight(g)	
	d	D	D Tolerance (μm)	L	L Tolerance (μm)	D1	PCD	H	K	d1	d2				h
LF-06UU	6	12	0	19	0	28	20	5	22	3.5	6	3.1	21	27	8
LF-08UU	8	15	-11	24		32	24	5	25	3.5	6	3.1	28	40	16
LF-10UU	10	19	0	29		40	29	6	30	4.5	7.5	4.1	38	56	30
LF-12UU	12	21	-13	30		42	32	6	32	4.5	7.5	4.1	52	80	31.5
LF-16UU	16	28		37		48	38	6	37	4.5	7.5	4.1	79	120	69
LF-20UU	20	32	0	42		54	43	8	42	5.5	9	5.1	90	140	87
LF-25UU	25	40	-16	59	62	51	8	50	5.5	9	5.1	100	159	220	
LF-30UU	30	45		64	74	60	10	58	6.6	11	6.1	159	279	250	
LF-40UU	40	60	0	80	96	78	13	75	9	14	8.1	218	409	585	
LF-50UU	50	80	-19	100	116	98	13	92	9	14	8.1	389	808	1580	

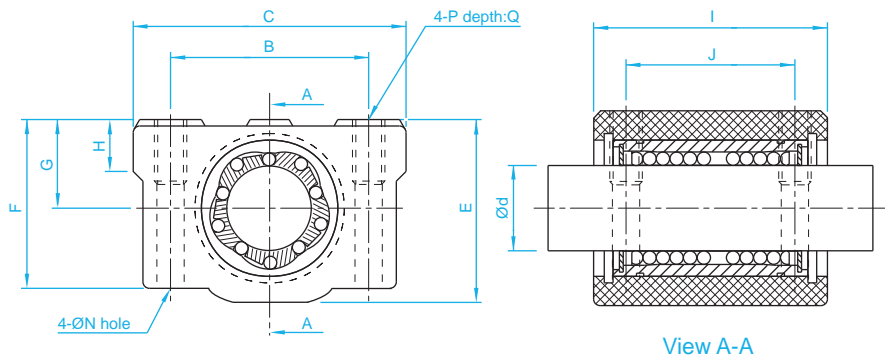
Model No.	Dimension											Ca (kgf)	Coa (kgf)	Weight(g)	
	d	D	D Tolerance (μm)	L	L Tolerance (μm)	D1	PCD	H	K	d1	d2				h
LF-06LUU	6	12	0	35	0	28	20	5	22	3.5	6	3.1	33	54	16
LF-08LUU	8	15	-13	45		32	24	5	25	3.5	6	3.1	44	80	31
LF-10LUU	10	19	0	55		40	29	6	30	4.5	7.5	4.1	60	112	62
LF-12LUU	12	21	-16	57		42	32	6	32	4.5	7.5	4.1	83	160	80
LF-16LUU	16	28		70		48	38	6	37	4.5	7.5	4.1	126	240	145
LF-20LUU	20	32	0	80		54	43	8	42	5.5	9	5.1	143	280	180
LF-25LUU	25	40	-19	112	62	51	8	50	5.5	9	5.1	159	320	440	
LF-30LUU	30	45		123	74	60	10	58	6.6	11	6.1	254	560	580	
LF-40LUU	40	60	0	151	96	78	13	75	9	14	8.1	350	820	1170	
LF-50LUU	50	80	-22	192	116	98	13	92	9	14	8.1	620	1622	3100	

※UU with oil seals in ends ※

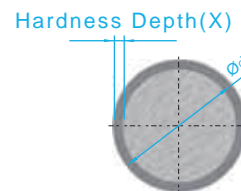
※UU with oil seals in ends ※

LINEAR BALL BEARING

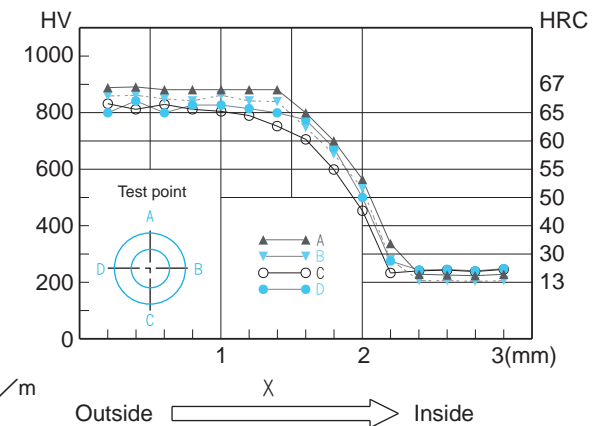
LU/LP Series Specifications (Aluminum Housing Type)



SF/WV Series Specifications (Shaft)



Material : CF53/S55C/SUJ2  
 Hardness : HRC60Up  
 Surface : Ra0.15-0.35µm  
 Shaft Straightness : approx.0.1mm/m



Unit : mm

Model No.	Dimension												Weight(g)
	d	B	C	E	F	G ±0.02	H	I	J	N	P	Q	
LU-08UU LP-08	8	24	34	22	18	11	6	30	18	3	M4	8	56
LU-10UU LP-10	10	28	40	26	21	13	8	35	21	4	M5	12	90
LU-12UU LP-12	12	30.5	42	29	25	15	8	36	26	4	M5	12	112
LU-16UU LP-16	16	36	50	38.5	35	19	9	44	34	4	M5	12	189
LU-20UU LP-20	20	40	54	42	36	21	11	50	40	5	M6	12	237
LU-25UU LP-25	25	54	76	51.5	41	26	12	67	50	6	M8	18	555
LU-30UU LP-30	30	58	78	59.5	49	30	15	72	58	6	M8	18	685
LU-40UU LP-40	40	80	102	78	62	40	20	90	60	8	M10	25	1600
LU-50UU LP-50	50	100	122	102	80	52	25	110	80	8	M10	25	3350

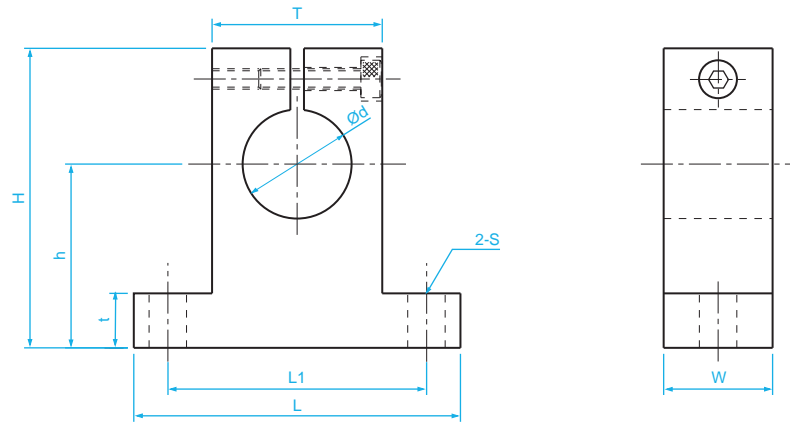
※LP-No Linear ball bearing is included.※

Unit : mm

Model No.	d	Hardness Depth (X)
★ SF-04	4	1.0
★ SF-06	6	1.0
★ SF-08	8	1.0
★ SF-10	10	1.0
★ SF-12	12	1.6
★ SF-16	16	1.6
★ SF-20	20	2.2
★ SF-25	25	2.2
★ SF-30	30	2.2
★ SF-32	32	2.2
★ SF-40	40	3.5
★ SF-50	50	3.5

※★ can supply Chromium plated slide shaft (Model No. WV).※

SS Series Specifications (Shaft Support)



Unit : mm

Model No.	Dimension									Weight(g)
	d	h	L	W	H	t	T	L1	S	
SS-04	4	20	42	14	32.8	6	18	32	5.5	24
SS-06	6	20	42	14	32.8	6	18	32	5.5	24
SS-08	8	20	42	14	32.8	6	18	32	5.5	24
SS-10	10	20	42	14	32.8	6	18	32	5.5	24
SS-12	12	23	42	14	37.5	6	20	32	5.5	30
SS-16	16	27	48	16	44	8	25	38	5.5	40
SS-20	20	31	60	20	51	10	30	45	6.6	70
SS-25	25	35	70	24	60	12	38	56	6.6	130
SS-30	30	42	84	28	70	12	44	64	9	180
SS-40	40	60	114	36	96	15	60	90	11	420
SS-50	50	70	126	40	120	18	74	100	14	750